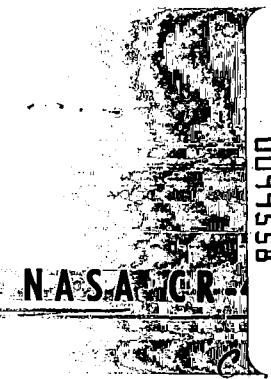
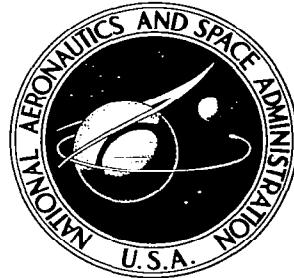


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**TABLES OF NATURAL FREQUENCIES
AND NODES FOR TRANSVERSE
VIBRATION OF TAPERED BEAMS**

by Han-chung Wang and Will J. Worley

Prepared under Grant No. NsG-434 by
UNIVERSITY OF ILLINOIS
Urbana, Ill.
for

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FOR TRANSVERSE VIBRATION OF TAPERED BEAMS

by

Han-chung Wang and Will J. Worley

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Urbana, Illinois

SUMMARY

The natural frequencies, nodal points and mode functions for transverse vibration of tapered beams are presented in this report.

The beams considered have the cross-sectional area bounded by the curve

$$\left| \frac{y}{h} \right|^{\beta} + \left| \frac{z}{b} \right|^{\gamma} = 1$$

with the thickness h and width b varying along the beam according to the relations

$$h = h_0 \left(\frac{x}{l} \right)^{\phi} \quad \text{and} \quad b = b_0 \left(\frac{x}{l} \right)^{\psi}$$

where β , γ , ϕ and ψ are positive constants not necessarily integers.



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INTRODUCTION

1. Statement of the Problem

The geometrical properties of solid bodies generated by revolving the line defined as

$$\left| \frac{x}{\ell} \right|^{\alpha} + \left| \frac{y}{h} \right|^{\beta} = 1 \quad (4.1)^*$$

and of bodies bounded by the surface defined as

$$\left| \frac{x}{\ell} \right|^{\alpha} + \left| \frac{y}{h} \right|^{\beta} + \left| \frac{z}{b} \right|^{\gamma} = 1 \quad (4.2)$$

have been published in the first and second reports [1, 2] ** under this grant. The current report treats the dynamic response of a general class of tapered beams. The shape of beams includes the bodies generated by Eqs. (4.1) and (4.2) with the parameter $\alpha = 1$. Special cases of bodies of the above shapes have been tested widely in NACA and NASA reports as well as in the technical journals, [3, 4, 5, 6, 7]. Beams of special shapes also have been applied as designs for high speed machine guns as reported in a recent paper by Elder [8].

To achieve more nearly complete information on the applications of this class of bodies, the results for the mode functions and for the natural frequencies of vibration of tapered beams are presented in this report. This report includes much of the existing data as special cases. The results appear in tables and in graphical form. The complete and detailed derivations are reported by Wang [9].

2. Profiles of the Beams

The beams whose flexural rigidity and mass per unit length vary according to two arbitrary powers of the longitudinal coordinate are considered in this report. The relationship of the variations may be written as

$$EI = E_0 I_0 \left(\frac{x}{\ell} \right)^m$$
$$\rho A = \rho_0 A_0 \left(\frac{x}{\ell} \right)^n \quad (4.3)$$

* The notation (4.1) is adopted to aid in cross-referencing equations from the first three reports under this grant.

** Number in brackets refer to the References.

where $E_o I_o$ is the bending rigidity and $\rho_o A_o$ is the mass per unit length at the larger end of the beam where $X = \ell$.

The relations of Eq. (4.3) can be considered as a homogeneous beam with the moment of inertia and cross-sectional area varying with powers m and n respectively. The relations can be applied for a general class of cross-sections with varying thickness and varying width. An important group of beam shapes can be considered as shown in Fig. 1. The cross-section of the beam is symmetrical and its first quadrant is bounded by the curve of the equation

$$\left(\frac{y}{h}\right)^\beta + \left(\frac{z}{b}\right)^\gamma = 1 \quad (4.4)$$

where b represents half of the width and h represents half of the thickness of the beam. These parameters vary according to the relations

$$b = b_o \left(\frac{X}{\ell}\right)^\psi, \quad h = h_o \left(\frac{X}{\ell}\right)^\phi \quad (4.5)$$

The constants ψ and ϕ are positive but not necessarily integers.

The selection of different values for the parameters γ and β in Eq. (4.4) permits the cross-section of the beam to be varied from the diamond shape, $\gamma = \beta = 1$, through the elliptical shape, $\gamma = \beta = 2$, to the rectangular shape, γ and $\beta \gg 1$. The moment of inertia and the area for this group of cross-section may be expressed in terms of γ and β [10], which gives

$$I = \frac{4}{3} b_o h_o^3 \left[\frac{\Gamma(\frac{1}{\gamma} + 1) \Gamma(\frac{3}{\beta} + 1)}{\Gamma(\frac{1}{\gamma} + \frac{3}{\beta} + 1)} \right] \left(\frac{X}{\ell}\right)^{\psi+3\phi} \quad (4.6)$$

$$A = 4b_o h_o \left[\frac{\Gamma(\frac{1}{\gamma} + 1) \Gamma(\frac{1}{\beta} + 1)}{\Gamma(\frac{1}{\gamma} + \frac{1}{\beta} + 1)} \right] \left(\frac{X}{\ell}\right)^{\psi+\phi}$$

Comparison of Eqs. (4.6) with Eqs. (4.3) yields the relationships

$$m = \psi + 3\phi, \quad n = \psi + \phi$$

The beam described by Eqs. (4.3) can also be considered as a nonhomogeneous beam with uniform cross-section, provided the modulus of elasticity and the density vary as powers m and n . The longitudinal vibration of beams of this type has been treated by Lindholm and Doshi [11].

3. Symbols

X	horizontal coordinate along the length of the beam
y	vertical coordinate perpendicular to X
z	horizontal coordinate perpendicular to X
ℓ	reference length of the beam
L	actual beam length
b	half the width of the beam
h	half the thickness of the beam
b_o	the width of the beam at the larger end
h_o	the thickness of the beam at the larger end
x	dimensionless abscissa, X/ℓ
α	exponent of (X/ℓ)
β	exponent of (y/h)
γ	exponent of (z/b)
ψ	exponent of x for width variation
ϕ	exponent of x for thickness variation
m	exponent of x for area moment of inertia variation
n	exponent of x for cross-sectional area variation
EI	bending rigidity of the beam (elastic modulus times moment of inertia of the cross-section)
ρA	mass per unit length of the beam
θ	$= 4 - m + n$
u	x^θ
δ_x	$x \frac{d}{dx}$
δ_u	$u \frac{d}{du}$
ω	circular frequency
p	eigenvalue , $\rho A_o \ell^4 \omega^2 / (EI_o)$
s	indicial root
${}_0F_3$	generalized hypergeometric function
$y(x)$	mode function

$U(x, \xi)$	influence function for beam deflections
$K(x, \xi)$	kernel of homogeneous integral equations
c	truncation of the beam, dimensionless; see Fig. 1
a_r	coefficients of the series
$P_u Q_v$	$\delta^u P \ \delta^v Q - \delta^v P \ \delta^u Q$
r_g	radius of gyration

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Both the ILLIAC II and the IBM 7094 computer facilities were used. The ILLIAC II was constructed in the Digital Computer Laboratory, now known as the Department of Computer Science, University of Illinois with support from the Atomic Energy Commission, grant USAEC AT(11-1)-415, and from the Office of Naval Research, grant NONOR-1832 (15). The IBM 7094 computer facility is partially supported by the National Science Foundation under NSF GP 700.

SOLUTIONS OF MODE FUNCTIONS

Neglecting rotatory inertia, the differential equation for the mode functions of vibrating beams is given as

$$\frac{d^2}{dx^2} EI(X) \frac{d^2y}{dx^2} - \rho\omega^2 A(X) y = 0 \quad (4.7)$$

For a homogeneous beam, having the profile described by the relations

$$I = I_0 \left(\frac{x}{\ell}\right)^m \quad \text{and} \quad A = A_0 \left(\frac{x}{\ell}\right)^n \quad (4.8)$$

Eq. (4.7) can be expanded as

$$x^4 \frac{d^4y}{dx^4} + 2mx^3 \frac{d^3y}{dx^3} + m(m-1)x^2 \frac{d^2y}{dx^2} - px^\theta y = 0 \quad (4.9)$$

where $x = (X/\ell)$, $p = \rho A_0 \ell^4 \omega^2 / (EI_0)$ and $\theta = 4 - m + n$.

Upon introducing the differential operator δ_x to represent $x \frac{d}{dx}$, Eq. (4.9) may be written as

$$\delta_x (\delta_x - 1) (\delta_x + m - 2) (\delta_x + m - 3) y - px^\theta y = 0 \quad (4.10)$$

Let $u = x^\theta$ and let $\delta_u = u \frac{d}{du}$, thus $\delta_x^r y = \theta^r \delta_u^r y$

and Eq. (4.10) yields

$$\delta_u (\delta_u - \frac{1}{\theta}) (\delta_u + \frac{m-2}{\theta}) (\delta_u + \frac{m-3}{\theta}) y - \frac{p}{\theta^4} u y = 0 \quad (4.11)$$

Equation (4.11) is a type of generalized hypergeometric equation [12], which possesses a general solution with linear combinations of four generalized hypergeometric functions. It can be written as

$$y = A_1 y_0 + A_2 y_1 + A_3 y_{2-m} + A_4 y_{3-m} \quad (4.12)$$

where each series, in hypergeometric series notation, is defined as

$$\begin{aligned}
 y_0 &= {}_0F_3\left(-; 1 - \frac{1}{\theta}, 1 + \frac{m-2}{\theta}, 1 + \frac{m-3}{\theta}; \frac{p}{\theta^4} u\right) \\
 y_1 &= u^{\frac{1}{\theta}} {}_0F_3\left(-; 1 + \frac{1}{\theta}, 1 + \frac{m-1}{\theta}, 1 + \frac{m-2}{\theta}; \frac{p}{\theta^4} u\right) \\
 y_{2-m} &= u^{\frac{2-m}{\theta}} {}_0F_3\left(-; 1 - \frac{1}{\theta}, 1 - \frac{m-1}{\theta}, 1 - \frac{m-2}{\theta}; \frac{p}{\theta^4} u\right) \\
 y_{3-m} &= u^{\frac{3-m}{\theta}} {}_0F_3\left(-; 1 + \frac{1}{\theta}, 1 - \frac{m-2}{\theta}, 1 - \frac{m-3}{\theta}; \frac{p}{\theta^4} u\right)
 \end{aligned} \tag{4.13}$$

provided that m is not an integer. When m is an integer, then logarithmic terms appear in the general solution.

The solutions of the differential equation (4.10) also can be obtained by the standard series method, the method of Frobenius. The series in Eq. (4.12) will have the form

$$y_s = x^s \sum_{r=0}^{\infty} a_r x^{r\theta} \tag{4.14}$$

with the recurrence formula of the coefficients being

$$a_r = \frac{p}{(s+r\theta)(s+r\theta-1)(s+r\theta+m-2)(s+r\theta+m-3)} a_{r-1} \tag{4.15}$$

where $s = 0, 1, 2-m$ and $3-m$ are the roots of the indicial equation.

When the parameter m is an integer, then two equal roots of s may exist for the indicial equation or the denominator of the recurrence formula of Eq. (4.15) becomes zero. When equal roots occur, the series solutions of Eq. (4.13) are dependent on each other. When the denominator of the recurrence formula is zero, the series solutions are meaningless. In these cases, by applying the theorems due to Frobenius [13], the independent series solution for the repeated root, $s = s_0$, is

$$\begin{aligned}
 y_{s_0} &= \log x \cdot (y)_{s=s_0} \\
 &= x^{s_0} \sum_{r=1}^{\infty} \left[\sum_{\eta=1}^r \left(\frac{1}{s_0 + \eta\theta} + \frac{1}{s_0 + \eta\theta - 1} + \frac{1}{s_0 + \eta\theta + m - 2} + \frac{1}{s_0 + \eta\theta + m - 3} \right) \right] a_r x^{r\theta}
 \end{aligned} \tag{4.16}$$

The series solution for the root, $s = s_1$, which makes the recurrence formula of the coefficients undefined, is given by

$$y_{s_1} = \log x \cdot (y)_{s=s_1} + x^{s_1} \left\{ 1 + \sum_{r=1}^{\infty} \left[\frac{1}{s-s_1} - \sum_{\eta=1}^r \left(\frac{1}{s+\eta\theta} + \frac{1}{s+\eta\theta+1} + \frac{1}{s+\eta\theta+m-2} + \frac{1}{s+\eta\theta+m-3} \right) \right]_{s=s_1} a_r x^{r\theta} \right\} \quad (4.17)$$

Again, when $\theta = 0$, the series of Eq. (4.14), does not apply. For this case, the recurrence formula of the coefficients is again undefined; however, Eq. (4.10) is then of the Euler-Cauchy type for which a general solution always exists of the form

$$y = A_1 x^{s_1} + A_2 x^{s_2} + A_3 x^{s_3} + A_4 x^{s_4} \quad (4.18)$$

where s_1, s_2, s_3 , and s_4 are the roots of the auxiliary equation

$$s(s-1)(s+m-2)(s+m-3) - p = 0 \quad (4.19)$$

Vibration can occur only when Eq. (4.19) has two or four non-real roots. This condition introduces the trigonometric function of $\log x$ into the solution for y .

Suppose s_1, s_2 are two real roots and s_3, s_4 are two complex roots represented by $\alpha_1 \pm i\alpha_2$, then the solution for the normal function has the form

$$y = A_1 x^{s_1} + A_2 x^{s_2} + x^{\alpha_1} \left[A_3 \cos(\alpha_2 \log x) + A_4 \sin(\alpha_2 \log x) \right] \quad (4.20)$$

FREQUENCY EQUATIONS AND NODAL POINTS

To establish the frequency equations for tapered beams with different end conditions, two separate geometrical categories of beams are treated. First, the complete tapered beam, which is gradually narrowed toward a point, is considered. The end coordinates of the beam are 0 and ℓ . Next, the truncated beam, with end coordinates $c \cdot \ell$ and ℓ , as indicated in Fig. 1, is considered. The origin, for the truncated beam lies beyond the end of the beam and serves as a reference point for the variation of the area moment of inertia and for the cross-sectional area of the beam.

1. Complete Tapered Beams

Since one end of the beam is at the origin, the arbitrary constants A_3 and A_4 in the general solution, Eq. (4.12), must vanish if finite values exist for the deflection, moment and shear at the end $x = 0$. Hence, the general solution of the mode function for beams with any combination of parameters m and n can be written as

$$y = A_1 P + A_2 Q \quad (4.21)$$

where P and Q are the series of y_0 and y_1 as defined in Eq. (4.13). The frequency equation is then obtained using the boundary conditions at $X = \ell$, that is, at $x = 1$. Three different cases are considered below.

A. Cantilever Beams

The base of the beam is fixed and the tip is free. Both the deflection and slope vanish at $x = 1$. Application of the boundary conditions to Eq. (4.21) and elimination of the constants A_1 and A_2 yields the frequency equation

$$P \frac{dQ}{dx} - Q \frac{dP}{dx} = 0 , \quad \text{at } x = 1 \quad (4.22)$$

Representation of $\delta^u P \cdot \delta^v Q - \delta^v P \cdot \delta^u Q$ in symbolic form as $P_u Q_v$ yields the relations $P_u Q_v = -P_v Q_u$ and $\delta(P_u Q_{u+1}) = P_u Q_{u+2}$. Using this notation, the frequency equation yields

$$\frac{1}{x} PQ_1 = 0 , \quad \text{at } x = 1 \quad (4.23)$$

Since P and Q are in series form, as in Eq. (4.14), their derivatives and products are in series form as well.

Let the series be defined as $U = PQ_1$. Then U is a solution of a fifth order differential equation

$$(\delta-1)(\delta+m-2)(\delta+m-3)(\delta+m-4)(\delta+2m-5)U + 2(2\delta+\theta+2m-6)p \frac{d^{\theta}}{dx^{\theta}}U = 0 \quad (4.24)$$

Solving Eq. (4.24) and comparing the corresponding terms of U with Eq. (4.23) the series which satisfies both Eq. (4.24) and (4.23) is established as

$$U = \sum_{r=0}^{\infty} a_r p^r x^{1+r\theta} \quad (4.25)$$

Substitution of U into Eq. (4.23) yields the frequency equation as a polynomial of p

$$\sum_{r=0}^{\infty} a_r p^r = 0 \quad (4.26)$$

with the recurrence formula of coefficients

$$a_r = \frac{-2(2r\theta - \theta + 2m - 4)}{r\theta(r\theta + m - 1)(r\theta + m - 2)(r\theta + m - 3)(r\theta + 2m - 4)} a_{r-1} \quad (4.27)$$

B. Antisymmetrical Mode Vibration of Free-Free Beams

Tapered beams with both ends free are considered to consist of two equal halves fitted together at their large ends as shown in Fig. 2. Each half is a section of a solid which has the profile shown in Fig. 1. When the beam vibrates in the antisymmetrical mode, the deflection and the bending moment are zero at the middle section where the two halves are joined together, that is

$$y = 0 \quad \text{and} \quad EI(x) \frac{d^2y}{dx^2} = 0 \quad \text{at } x = 1$$

Substitution of these conditions into Eq. (4.21) and applying the differential operator $P_u Q_v$, the frequency equation becomes

$$\frac{1}{x^2} U = 0 \quad \text{at } x = 1 \quad (4.28)$$

where $U = PQ_2 - PQ_1$. The function U is a solution of a fifth order differential

equation

$$(\delta - \theta - 1)(\delta + m - 4)(\delta + m - 3)(\delta + 2m - 5)(\delta + m - 2)U + 2(2\delta + \theta + 2m - 6)p_x^\theta U = 0 \quad (4.29)$$

Hence, the frequency equation may again be represented by a polynomial of p_i , of the form of Eq. (4.26), with the coefficients

$$a_r = \frac{-2(2r\theta + \theta + 2m - 4)}{r\theta(r\theta + \theta + m - 1)(r\theta + \theta + m - 2)(r\theta + \theta + m - 3)(r\theta + \theta + 2m - 4)} a_{r-1} \quad (4.30)$$

The locations of the nodes for the normal mode vibration, can be obtained by substituting the corresponding natural frequency, p_i , into Eq. (4.21) and solving for x with y equal to zero. Since P and Q are generalized hypergeometric functions, the equation, which gives the nodal points for cantilever beams and free-free beams of antisymmetrical mode, can be represented by

$${}_0F_3(-; 1 + \frac{1}{\theta}, 1 + \frac{m-1}{\theta}, 1 + \frac{m-2}{\theta}; \frac{p_i}{\theta^4}) {}_0F_3(-; 1 - \frac{1}{\theta}, 1 + \frac{m-2}{\theta}, 1 + \frac{m-3}{\theta}; p_i \frac{x^\theta}{\theta^4}) \\ - x {}_0F_3(-; 1 - \frac{1}{\theta}, 1 + \frac{m-2}{\theta}, 1 + \frac{m-3}{\theta}; \frac{p_i}{\theta^4}) {}_0F_3(-; 1 + \frac{1}{\theta}, 1 + \frac{m-1}{\theta}, 1 + \frac{m-2}{\theta}; p_i \frac{x^\theta}{\theta^4}) = 0 \quad (4.31)$$

C. Symmetrical Mode Vibration of Free-Free Beams

For the symmetrical mode vibration of the free-free beam, Fig. 2, the slope and shear are zero at the middle section of the beam, hence

$$\frac{dy}{dx} = 0 \quad \text{and} \quad \frac{d}{dx} EI(x) \frac{d^2y}{dx^2} = 0 \quad \text{at } x = 1$$

Upon substituting the end conditions into Eq. (4.21) and using the notation $P_u Q_v$, the frequency equation may be written as

$$\frac{d}{dx}(x^{m-3}U) = 0 \quad (4.32)$$

at $x = 1$, where

$$U = PQ_3 + (m-3)PQ_2 - (m-2)PQ_1$$

As discussed in the previous sections, U may be represented by a series which is a solution of a sixth order differential equation

$$\begin{aligned} & (\delta - \theta - 1) (\delta - \theta + m - 2) (\delta - \theta + m - 3) (\delta + m - 4) (\delta + m - 3) (\delta + 2m - 5) U \\ & + 2(2\delta + \theta + 2m - 6) (\delta + m - 3) p x^\theta U = 0 \end{aligned} \quad (4.33)$$

Substituting the solution U into Eq. (4.32) and evaluating at $x = 1$, gives the equation for the eigenvalues p as

$$\sum_{r=0}^{\infty} (r\theta + \theta + m - 2) a_r p^r = 0 \quad (4.34)$$

with the recurrence formulas for the coefficients

$$a_r = \frac{-2(2r\theta + \theta + 2m - 4)}{r\theta(r\theta + m - 1)(r\theta + \theta + m - 2)(r\theta + \theta + m - 3)(r\theta + \theta + 2m - 4)} a_{r-1} \quad (4.35)$$

The locations of the nodes for the normal mode vibration in this case can be solved from the equation

$$\begin{aligned} & \left[\frac{p_i}{(\theta+1)(\theta+m-1)(\theta+m-2)} {}_0F_3 \left(-; 2 + \frac{1}{\theta}, 2 + \frac{m-1}{\theta}, 2 + \frac{m-2}{\theta}; \frac{p_i}{\theta^4} \right) \right. \\ & \left. + {}_0F_3 \left(-; 1 + \frac{1}{\theta}, 1 + \frac{m-1}{\theta}, 1 + \frac{m-2}{\theta}; \frac{p_i}{\theta^4} \right) \right] {}_0F_3 \left(-; 1 - \frac{1}{\theta}, 1 + \frac{m-2}{\theta}, 1 + \frac{m-3}{\theta}; p_i \frac{x^\theta}{\theta^4} \right) \\ & - \left[\frac{p_i x}{(\theta+1)(\theta+m-2)(\theta+m-3)} {}_0F_3 \left(-; 1 - \frac{1}{\theta}, 1 + \frac{m-2}{\theta}, 1 + \frac{m-3}{\theta}; \frac{p_i}{\theta^4} \right) \right. \\ & \left. {}_0F_3 \left(-; 1 + \frac{1}{\theta}, 1 + \frac{m-1}{\theta}, 1 + \frac{m-2}{\theta}; p_i \frac{x^\theta}{\theta^4} \right) \right] = 0 \end{aligned} \quad (4.36)$$

2. Truncated Tapered Beams

A. Exact Solutions

A beam which is gradually reduced to a small cross-section instead of to a point, may be considered as a beam truncated at the location $x = c$ as shown in Fig. 1. The total length of the beam is $(l - c) \cdot l$, where l is a reference length for the tapering. Since the beam does not start from the origin, the general solution of the mode function must be written in the form of Eq. (4.12) with four series. By substituting the end conditions into the mode function, a fourth order determinant equation of the eigenvalues p may be obtained.

Consider the case for a cantilever beam; the end conditions are

$$y = y' = 0 \quad \text{at } x = 1$$

$$\text{and } EIy'' = (EIy'')' = 0 \quad \text{at } x = c$$

which gives the frequency equation

$$\begin{vmatrix} [y_0]_{x=1} & [y_1]_{x=1} & [y_{2-m}]_{x=1} & [y_{3-m}]_{x=1} \\ [y'_0]_{x=1} & [y'_1]_{x=1} & [y'_{2-m}]_{x=1} & [y'_{3-m}]_{x=1} \\ [y''_0]_{x=c} & [y''_1]_{x=c} & [y''_{2-m}]_{x=c} & [y''_{3-m}]_{x=c} \\ [(x^m y''_0)']_{x=c} & [(x^m y''_1)']_{x=c} & [(x^m y''_{2-m})']_{x=c} & [(x^m y''_{3-m})']_{x=c} \end{vmatrix} = 0 \quad (4.37)$$

where y_0 , y_1 , y_{2-m} and y_{3-m} are defined by Eqs. (4.13), (4.16), or (4.17).

B. Approximate Solutions

The calculation of the natural frequencies from the characteristic equation, Eq. (4.37), involves tedious numerical computations since each element in the determinant is a combination of generalized hypergeometric series. For practical purposes and in order to supply results to check the exact solutions, two approximate methods are introduced for calculating the upper bound and the lower bound of the approximate fundamental frequencies.

The Ritz method is one of the approximate methods which has been widely used to determine the upper bound of the natural frequencies for elastic systems. The frequency of the fundamental mode is calculated by minimizing the expression for the energies, which, for beams having the prescribed profile is

$$P = \int_c^1 x^m \left(\frac{dy}{dx} \right)^2 dx / \int_c^1 x^n y^2 dx \quad (4.38)$$

As an example, consider a cantilever beam. In order to satisfy the boundary conditions at free end, a one term approximation is assumed for the second derivative of the beam deflection, as

$$y'' = 12a(x - c)^2 \quad (4.39)$$

Integration of Eq. (4.39) gives the deflection curve

$$y = a \left[(x - c)^4 + C_1 x + C_2 \right]$$

where $C_1 = -4(1 - c)^3$ and $C_2 = 4(1 - c)^3 - (1 - c)^4$ in order to satisfy the boundary conditions $y = y' = 0$ at $x = 1$.

The lower bound approximate frequency of the fundamental mode is obtained from the expression

$$p = 1 \int_c^1 K(x, \xi) d\xi \quad (4.41)$$

where

$$K(x, \xi) = \frac{EI_0}{\ell^3} \xi^n U(x, \xi) \quad (4.42)$$

is the kernel of a homogeneous integral equation for the beam profile of current interest. The influence function for beam deflections, $U(x, \xi)$, is the static deflection of the beam at x with a unit load applied at a distance ξ measured from the origin. For a cantilever beam, $U(x, \xi)$ can be expressed as

$$U(x, \xi) = \frac{\ell^3}{EI_0} \left[\frac{1}{(2-m)(3-m)} x^{3-m} - \frac{\xi}{(1-m)(2-m)} x^{2-m} + \frac{(2-m)\xi - (1-m)}{(1-m)(2-m)} x - \frac{(3-m)\xi - (2-m)}{(2-m)(3-m)} \right] \quad (4.43)$$

for $m \neq 1, 2$ and 3 , and

$$\begin{aligned} U(x, \xi) &= \frac{\ell^3}{EI_0} \left[\frac{x^2}{2} - \xi x (\log x - 1) - x - \xi + \frac{1}{2} \right], & \text{for } m = 1 \\ U(x, \xi) &= \frac{\ell^3}{EI_0} \left[x(\log x - 1) + \xi(\log x - x) + \xi + 1 \right], & \text{for } m = 2 \quad (4.44) \\ U(x, \xi) &= \frac{\ell^3}{EI_0} \left[x \left(1 - \frac{\xi}{2}\right) - \log x - \frac{\xi}{2x} + \xi - 1 \right], & \text{for } m = 3 \end{aligned}$$

NUMERICAL RESULTS AND DISCUSSION OF TABLES

1. Natural Frequencies and Nodal Points for Complete Tapered Beams

The natural frequencies for different vibrational modes of complete tapered beams can be calculated by solving for the roots of polynomials of Eqs. (4.26) and (4.34). The coefficients of the polynomials, for cantilever beams, for free-free beams executing antisymmetrical vibrational modes and for free-free beams executing symmetrical vibrational modes, can be generated from Eqs. (4.27), (4.30) and (4.35) respectively. The recurrence formulas indicate that the coefficients reduce rapidly as the number of terms increases. Therefore, in the numerical calculations, the first five frequencies are computed with the first sixteen terms of the series. Computer programs are written to generate the coefficients as well as to solve for the roots.

The exponents, for a uniform beam, are $\psi = \phi = 0$ or $m = 0$, $\theta = 4$, and the frequency equation for cantilever beams, Eq. (4.26), becomes

$$\sum_{r=0}^{\infty} \frac{(-1)^r}{(4r)!} (4p)^r = 0 \quad (4.45)$$

where $p = \omega^2 \left(\frac{\rho A_0}{E I_0} \right) l^4$ as defined earlier. Let the beam length be L , which is equal to l_0 for the complete tapered beam, and let the frequency constant K be \sqrt{p} . Then the natural frequency can be represented as

$$\omega = K \sqrt{\frac{E I_0}{\rho A_0}} / L^2 \quad (4.46)$$

The first five frequency constants, K , for uniform cantilever beams are obtained from Eq. (4.45) using the first 16 terms of the series. These frequency constants are

$$3.51601, \quad 22.0345, \quad 61.6972, \quad 120.911, \quad 199.860$$

The substitution of each frequency into Eq. (4.31) establishes the locations the nodes for the corresponding natural frequency, which are given in the following table.

Uniform Cantilever Beam

ψ	ϕ	mode	frequency constant; K	locations of nodes, (X/L)			
				1st	2nd	3rd	4th
.00	.00	1st	3.51601	1.00000			
		2nd	22.03449	.21656	1.00000		
		3rd	61.69721	.13232	.49645	1.00000	
		4th	120.90191	.09444	.35591	.64166	1.00000
		5th	199.85953	.07345	.27678	.50009	.72125
							1.00000

In the table, the first two columns display the combinations of the exponents ψ and ϕ , the third and fourth columns indicate corresponding modes and their natural frequencies. The remaining columns show the locations of the nodes for different modes.

For cantilever beams with other combinations of ψ and ϕ , the results for frequencies and nodes for the first five modes are listed in Table 1. Page one of Table 1 lists data for the combinations of ψ and ϕ corresponding to beams of constant thickness with width varying as x^ψ . Page two of the table lists corresponding data for beams of constant width with thickness varying as x^ϕ . The frequency data of these two cases are also plotted in Figs. 3 and 4 as the ratio of frequencies of tapered beams to those of uniform beams. Fig. 5 indicates the variation of the ratio of frequencies for the beams with taper both in width and thickness according to x^ϕ . The ratio of frequencies for the first three modes, for 81 combinations of ψ and ϕ , are plotted in Fig. 6 in three dimensional form. The figures reveal the variation of the natural frequencies of different modes as the taper of the beam varies. It is of interest to note that the frequencies of the fundamental mode increase when the beams taper either in width or in thickness. The frequencies of the higher modes increase as the taper of the width increases, that is, as ψ decreases. The higher mode frequencies decrease as the taper on the thickness increases, that is, as ϕ increases.

The shapes of the first four normal modes for the vibration of tapered cantilever beams are plotted in Figs. 7, 8 and 9. Fig. 7 shows the change of mode shapes and the shifting of the nodal points for constant thickness beams as the exponent ψ increases. Fig. 8 shows those for beams with constant width and varying thickness. Fig. 9 displays those for beams with both width and thickness varying as a same power of x , that is $\psi = \phi$. The amplitudes of the deflections are normalized to the deflection at the free end.

For free-free beams of antisymmetrical and symmetrical mode vibration, the frequency constant K and the nodal points are also computed. For a uniform free-free beam, vibrating in antisymmetrical modes, the frequencies can be obtained from Eq. (4.26) with coefficients given by Eq. (4.30) and with $m = 0, n = 4$, that is

$$\sum_{r=0}^{\infty} \frac{(-1)^r}{(4r+3)!} (4p)^r = 0 \quad (4.47)$$

The substitution of the first five roots of Eq. (4.47) into Eq. (4.31) gives the locations of the nodes for the corresponding mode. The results are listed as follows:

Uniform Free-Free Beam of Antisymmetrical Mode

ψ	ϕ	mode	frequency		locations of nodes (X/L)	
			constant, K			
.00	.00	1st	5.59332	.44832		
		2nd	30.22585	.18889	.71161	
		3rd	74.63888	.12020	.45291	.81825
		4th	138.79131	.08814	.33213	.60005 .86666
		5th	222.68295	.06959	.26221	.47372 .68421 .89474

The results for other combinations of ψ and ϕ are listed in Table 2 in the same order as in Table 1. The variation of the ratio of the frequencies of tapered beams to the frequencies of uniform beams are plotted in Fig. 10. The nodal points listed here are for one half of the beam length. The nodes of the other half of the beam are symmetrically located. The notation L represents half the total length of the free-free beam.

For free-free beams of symmetrical mode vibration, the frequencies and nodal points are evaluated from Eqs. (4.34) and (4.36) respectively. The results are listed in Table 3. For a uniform beam, the frequency equation is given as

$$\sum_{r=0}^{\infty} \frac{(-1)^r}{(4r+1)!} (4p)^r = 0 \quad (4.48)$$

which gives the first five roots and the corresponding nodes as follows:

Uniform Free-Free Beam of Symmetrical Mode

ψ	ϕ	mode	frequency		locations of nodes (X/L)		
			constant, K				
.00	.00	1st	15.41821	.2642	1.0000		
		2nd	49.96486	.1469	.5536	1.0000	
		3rd	104.24769	.1017	.3832	.6924	1.0000
		4th	178.26972	.0778	.2931	.5295	.7647 1.0000
		5th	272.03098	.0630	.2372	.4286	.6190 .8095 1.0000

The above calculated results for frequencies and nodes for general tapered beams are checked with existing results of some special cases which appear in References [14, 15, 16, 17, 18, 19, 20].

2. Natural Frequencies of Truncated Beams

For truncated cantilever beams the frequency constants, K in Eq. (4.46), are the roots of Eq. (4.37). The numerical results are obtained by using the method of regula falsi. The series involved in each of the elements of Eq. (4.37) are calculated using 16 terms. The frequency constants K for the first two vibrational modes are presented in Table 4 for beams truncated at 0.2ℓ and at 0.4ℓ . The combinations of the exponents ψ and ϕ again include the beams with constant thickness, with constant width and with both thickness and width varying as the same power.

The upper bound and the lower bound approximations for the fundamental natural frequencies are calculated for six different degrees of truncation as well as for complete tapered beams. The values for the lower bound approximation are evaluated from Eq. (4.41) with the kernel defined in Eq. (4.42). The values of the upper bound approximation are evaluated from Eq. (4.38) with the deflection curve defined as Eq. (4.40). The approximate values of K are listed in Table 5 with 84 different combinations of ψ and ϕ .

Comparisons of the correct frequencies of truncated beams with the approximate frequencies appear in Figs. 12, 13 and 14. The results for constant thickness beams with varying width appear in Fig. 12, while Fig. 13 displays results for constant width beams with varying thickness and Fig. 14 gives the results for beams for which both width and thickness vary. The frequencies of the upper bound approximation for constant thickness beams are closer to the correct results than those for constant width beams. This implies that the assumed deflection curve is more nearly correct for the constant thickness beams. The lower bound approximations also yield more nearly

correct results for beams with constant thickness than for beams with constant width. This is true because the frequencies of the higher modes for constant thickness beams are larger than those for constant width beams.

3. Radii of Gyration of Cross-Section

The evaluation of circular frequencies from the frequency constants K , as defined in Eq. (4.46), involves the calculation of the radius of gyration, $(I_o/A_o)^{1/2}$. For the beams with cross-sections bounded by Eq. (4.4), the area moments of inertia and the cross-sectional areas with different values of γ and β were listed in the first report [1]. The radius of gyration of the cross-section at the large end of the beam, calculated from Eq. (4.6), is

$$\frac{r_g}{h_o} = \frac{1}{3} - \frac{\left(\frac{3}{\beta} + 1\right) \left(\frac{1}{\gamma} + \frac{1}{\beta} + 1\right)}{\left(\frac{1}{\beta} + 1\right) \left(\frac{1}{\gamma} + \frac{3}{\beta} + 1\right)} \quad (4.49)$$

The results of Eq. (4.49) are listed in Table 6 with the same combinations of α and β as those used in the first report.

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TABLE 1. NATURAL FREQUENCIES AND NODES FOR TAPERED CANTILEVER BEAMS

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.10	.00	1ST	3.84759	1.00000			
		2ND	22.91518	.23054	1.00000		
		3RD	63.04715	.14189	.50266	1.00000	
		4TH	122.74233	.10160	.36153	.64453	1.00000
		5TH	202.19116	.07916	.28164	.50319	.72293 1.00000
.20	.00	1ST	4.18617	1.00000			
		2ND	23.79954	.24375	1.00000		
		3RD	64.40342	.15105	.50861	1.00000	
		4TH	124.58941	.10851	.36696	.64732	1.00000
		5TH	204.52963	.08469	.28636	.50624	.72459 1.00000
.30	.00	1ST	4.53188	1.00000			
		2ND	24.68792	.25626	1.00000		
		3RD	65.76605	.15985	.51432	1.00000	
		4TH	126.44310	.11519	.37221	.65005	1.00000
		5TH	206.87497	.09006	.29095	.50922	.72621 1.00000
.40	.00	1ST	4.88482	1.00000			
		2ND	25.58063	.26812	1.00000		
		3RD	67.13513	.16831	.51982	1.00000	
		4TH	128.30356	.12166	.37731	.65272	1.00000
		5TH	209.22717	.09527	.29542	.51215	.72781 1.00000
.50	.00	1ST	5.24506	1.00000			
		2ND	26.47796	.27941	1.00000		
		3RD	68.51067	.17647	.52511	1.00000	
		4TH	130.17072	.12793	.38225	.65533	1.00000
		5TH	211.58626	.10035	.29977	.51502	.72938 1.00000
.60	.00	1ST	5.61263	1.00000			
		2ND	27.38015	.29017	1.00000		
		3RD	69.89271	.18434	.53022	1.00000	
		4TH	132.04458	.13402	.38705	.65788	1.00000
		5TH	213.95227	.10529	.30402	.51783	.73092 1.00000
.80	.00	1ST	6.36984	1.00000			
		2ND	29.19990	.31028	1.00000		
		3RD	72.67645	.19930	.53992	1.00000	
		4TH	135.81270	.14570	.39625	.66281	1.00000
		5TH	218.70500	.11482	.31221	.52331	.73394 1.00000
1.00	.00	1ST	7.15646	1.00000			
		2ND	31.04131	.32874	1.00000		
		3RD	75.48660	.21333	.54900	1.00000	
		4TH	139.60798	.15678	.40498	.66755	1.00000
		5TH	223.48545	.12392	.32004	.52860	.73685 1.00000

TABLE 1. NATURAL FREQUENCIES AND NODES FOR TAPERED CANTILEVER BEAMS

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.00	.10	1ST	3.75540	1.00000			
		2ND	21.53823	.22510	1.00000		
		3RD	58.22532	.13605	.49123	1.00000	
		4TH	112.59111	.09607	.34845	.63288	1.00000
		5TH	184.78438	.07402	.26843	.48864	.71254 1.00000
.00	.20	1ST	3.98423	1.00000			
		2ND	20.99322	.23211	1.00000		
		3RD	54.81987	.13863	.48536	1.00000	
		4TH	104.54557	.09677	.34037	.62355	1.00000
		5TH	170.27172	.07380	.25953	.47657	.70323 1.00000
.00	.30	1ST	4.20172	1.00000			
		2ND	20.40273	.23769	1.00000		
		3RD	51.48127	.14012	.47883	1.00000	
		4TH	96.76554	.09660	.33162	.61360	1.00000
		5TH	156.32171	.07285	.25005	.46380	.69324 1.00000
.00	.40	1ST	4.40698	1.00000			
		2ND	19.76973	.24191	1.00000		
		3RD	48.20998	.14058	.47157	1.00000	
		4TH	89.25128	.09560	.32216	.60296	1.00000
		5TH	142.93450	.07123	.23998	.45027	.68250 1.00000
.00	.50	1ST	4.59896	1.00000			
		2ND	19.09684	.24483	1.00000		
		3RD	45.00642	.14003	.46353	1.00000	
		4TH	82.00310	.09381	.31196	.59156	1.00000
		5TH	130.11026	.06896	.22928	.43590	.67089 1.00000
.00	.60	1ST	4.77655	1.00000			
		2ND	18.38646	.24647	1.00000		
		3RD	41.87105	.13849	.45463	1.00000	
		4TH	75.02126	.09126	.30096	.57928	1.00000
		5TH	117.84916	.06610	.21793	.42060	.65832 1.00000
.00	.80	1ST	5.08332	1.00000			
		2ND	16.86125	.24588	1.00000		
		3RD	35.80663	.13245	.43390	1.00000	
		4TH	61.85787	.08395	.27624	.55160	1.00000
		5TH	95.01719	.05871	.19314	.38675	.62966 1.00000
.00	1.00	1ST	5.31510	1.00000			
		2ND	15.29717	.23980	1.00000		
		3RD	30.01981	.12230	.40833	1.00000	
		4TH	49.76335	.07376	.24730	.51858	1.00000
		5TH	74.44003	.04931	.16529	.34763	.59497 1.00000

TABLE 1. NATURAL FREQUENCIES AND NODES FOR TAPERED CANTILEVER BEAMS

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.10	.10	1ST	4.08637	1.00000			
		2ND	22.38253	.23812	1.00000		
		3RD	59.52071	.14497	.49731	1.00000	
		4TH	114.35302	.10272	.35396	.63583	1.00000
		5TH	187.01330	.07930	.27318	.49183	.71431 1.00000
.10	.20	1ST	4.31441	1.00000			
		2ND	21.80267	.24428	1.00000		
		3RD	56.06091	.14698	.49135	1.00000	
		4TH	106.22908	.10297	.34578	.62659	1.00000
		5TH	172.39803	.07869	.26418	.47984	.70509 1.00000
.10	.30	1ST	4.53085	1.00000			
		2ND	21.17865	.24911	1.00000		
		3RD	52.66817	.14797	.48473	1.00000	
		4TH	98.37077	.10239	.33694	.61674	1.00000
		5TH	158.34546	.07739	.25461	.46715	.59520 1.00000
.10	.40	1ST	4.73475	1.00000			
		2ND	20.51322	.25268	1.00000		
		3RD	49.34290	.14797	.47741	1.00000	
		4TH	90.77835	.10102	.32741	.60621	1.00000
		5TH	144.85576	.07544	.24444	.45371	.68456 1.00000
.10	.50	1ST	4.92505	1.00000			
		2ND	19.80887	.25501	1.00000		
		3RD	46.08556	.14700	.46932	1.00000	
		4TH	83.45211	.09889	.31714	.59491	1.00000
		5TH	131.92909	.07287	.23366	.43943	.67307 1.00000
.10	.60	1ST	5.10058	1.00000			
		2ND	19.06779	.25613	1.00000		
		3RD	42.89657	.14508	.46039	1.00000	
		4TH	76.39234	.09602	.30607	.58276	1.00000
		5TH	119.56565	.06973	.22222	.42421	.66062 1.00000
.10	.80	1ST	5.40200	1.00000			
		2ND	17.48294	.25464	1.00000		
		3RD	36.72535	.13835	.43962	1.00000	
		4TH	63.07337	.08812	.28123	.55534	1.00000
		5TH	96.52915	.06181	.19723	.39055	.63226 1.00000
.10	1.00	1ST	5.62660	1.00000			
		2ND	15.77062	.24780	1.00000		
		3RD	30.83211	.12757	.41406	1.00000	
		4TH	50.82352	.07737	.25215	.52262	1.00000
		5TH	75.74766	.05191	.16916	.35161	.59792 1.00000

TABLE 1. NATURAL FREQUENCIES AND NODES FOR TAPERED CANTILEVER BEAMS

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)				
.20	.10	1ST	4.42440	1.00000				
		2ND	23.23123	.25045	1.00000			
		3RD	60.82253	.15355	.50316	1.00000		
		4TH	116.12162	.10917	.35930	.63871	1.00000	
		5TH	189.24912	.08443	.27781	.49495	.71605	1.00000
.20	.20	1ST	4.65164	1.00000				
		2ND	22.61712	.25585	1.00000			
		3RD	57.30847	.15504	.49712	1.00000		
		4TH	107.91934	.10900	.35103	.62956	1.00000	
		5TH	174.53124	.08346	.26871	.48304	.70691	1.00000
.20	.30	1ST	4.86701	1.00000				
		2ND	21.96005	.26001	1.00000			
		3RD	53.86166	.15556	.49043	1.00000		
		4TH	99.98279	.10804	.34212	.61980	1.00000	
		5TH	160.37614	.08183	.25905	.47043	.69712	1.00000
.20	.40	1ST	5.06950	1.00000				
		2ND	21.26259	.26298	1.00000			
		3RD	50.48250	.15514	.48305	1.00000		
		4TH	92.31226	.10633	.33252	.60938	1.00000	
		5TH	146.78397	.07957	.24880	.45707	.68658	1.00000
.20	.50	1ST	5.25804	1.00000				
		2ND	20.52706	.26479	1.00000			
		3RD	47.17144	.15379	.47492	1.00000		
		4TH	84.90802	.10388	.32219	.59819	1.00000	
		5TH	133.75492	.07673	.23794	.44288	.67521	1.00000
.20	.60	1ST	5.43143	1.00000				
		2ND	19.75552	.26542	1.00000			
		3RD	43.92890	.15151	.46596	1.00000		
		4TH	77.77034	.10071	.31106	.58615	1.00000	
		5TH	121.28914	.07332	.22641	.42775	.66289	1.00000
.20	.80	1ST	5.72734	1.00000				
		2ND	18.11131	.26311	1.00000			
		3RD	37.65095	.14413	.44517	1.00000		
		4TH	64.29584	.09224	.28610	.55898	1.00000	
		5TH	98.04816	.06490	.20125	.39427	.63480	1.00000
.20	1.00	1ST	5.94455	1.00000				
		2ND	16.34084	.25557	1.00000			
		3RD	31.65133	.13275	.41962	1.00000		
		4TH	51.89071	.08095	.25691	.52655	1.00000	
		5TH	77.06235	.05451	.17297	.35551	.60081	1.00000

TABLE 1. NATURAL FREQUENCIES AND NODES FOR TAPERED CANTILEVER BEAMS

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)				
.30	.10	1ST	4.76957	1.00000				
		2ND	24.08461	.26218	1.00000			
		3RD	62.13082	.16182	.50879	1.00000		
		4TH	117.89695	.11542	.36447	.64153	1.00000	
		5TH	191.49183	.08942	.28231	.49801	.71775	1.00000
.30	.20	1ST	4.99599	1.00000				
		2ND	23.43679	.26689	1.00000			
		3RD	58.56259	.16283	.50267	1.00000		
		4TH	109.61637	.11487	.35613	.63246	1.00000	
		5TH	176.67138	.08812	.27313	.48617	.70871	1.00000
.30	.30	1ST	5.21022	1.00000				
		2ND	22.74709	.27044	1.00000			
		3RD	55.06178	.16292	.49593	1.00000		
		4TH	101.60165	.11356	.34715	.62280	1.00000	
		5TH	162.41377	.08618	.26339	.47365	.69901	1.00000
.30	.40	1ST	5.41124	1.00000				
		2ND	22.01795	.27287	1.00000			
		3RD	51.62881	.16211	.48850	1.00000		
		4TH	93.85304	.11152	.33749	.61247	1.00000	
		5TH	148.71918	.08364	.25307	.46038	.68857	1.00000
.30	.50	1ST	5.59794	1.00000				
		2ND	21.25152	.27418	1.00000			
		3RD	48.26409	.16040	.48034	1.00000		
		4TH	86.37083	.10877	.32711	.60139	1.00000	
		5TH	135.58774	.08053	.24213	.44627	.67731	1.00000
.30	.60	1ST	5.76911	1.00000				
		2ND	20.44970	.27438	1.00000			
		3RD	44.96803	.15779	.47136	1.00000		
		4TH	79.15528	.10531	.31592	.58946	1.00000	
		5TH	123.01965	.07686	.23053	.43123	.66510	1.00000
.30	.80	1ST	6.05931	1.00000				
		2ND	18.74637	.27131	1.00000			
		3RD	38.58345	.14980	.45056	1.00000		
		4TH	65.52530	.09632	.29088	.56254	1.00000	
		5TH	99.57422	.06796	.20521	.39792	.63730	1.00000
.30	1.00	1ST	6.26895	1.00000				
		2ND	16.91781	.26312	1.00000			
		3RD	32.47746	.13786	.42504	1.00000		
		4TH	52.96490	.08451	.26158	.53040	1.00000	
		5TH	78.38411	.05711	.17672	.35934	.60365	1.00000

TABLE 1. NATURAL FREQUENCIES AND NODES FOR TAPERED CANTILEVER BEAMS

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.40	.10	1ST	5.12194	1.00000			
		2ND	24.94292	.27335	1.00000		
		3RD	63.44562	.16980	.51421	1.00000	
		4TH	119.67903	.12150	.36949	.64427	1.00000
		5TH	193.74142	.09429	.28670	.50101	.71943 1.00000
.40	.20	1ST	5.34749	1.00000			
		2ND	24.26185	.27743	1.00000		
		3RD	59.82330	.17037	.50803	1.00000	
		4TH	111.32020	.12059	.36108	.63529	1.00000
		5TH	178.81845	.09267	.27745	.48925	.71047 1.00000
.40	.30	1ST	5.56052	1.00000			
		2ND	23.53993	.28043	1.00000		
		3RD	56.26857	.17007	.50124	1.00000	
		4TH	103.22733	.11895	.35205	.62572	1.00000
		5TH	164.45835	.09045	.26764	.47681	.70086 1.00000
.40	.40	1ST	5.75999	1.00000			
		2ND	22.77940	.28236	1.00000		
		3RD	52.78184	.16889	.49378	1.00000	
		4TH	95.40070	.11661	.34234	.61549	1.00000
		5TH	150.66135	.08764	.25725	.46361	.69052 1.00000
.40	.50	1ST	5.94477	1.00000			
		2ND	21.98229	.28323	1.00000		
		3RD	49.36352	.16685	.48559	1.00000	
		4TH	87.84056	.11357	.33190	.60451	1.00000
		5TH	137.42756	.08427	.24624	.44959	.67937 1.00000
.40	.60	1ST	6.11362	1.00000			
		2ND	21.15039	.28303	1.00000		
		3RD	46.01401	.16393	.47659	1.00000	
		4TH	80.54718	.10985	.32068	.59269	1.00000
		5TH	124.75719	.08037	.23457	.43464	.66728 1.00000
.40	.80	1ST	6.39792	1.00000			
		2ND	19.38815	.27925	1.00000		
		3RD	39.52286	.15537	.45579	1.00000	
		4TH	66.76175	.10034	.29555	.56602	1.00000
		5TH	101.10733	.07100	.20910	.40151	.63975 1.00000
.40	1.00	1ST	6.59979	1.00000			
		2ND	17.50155	.27046	1.00000		
		3RD	33.31050	.14289	.43032	1.00000	
		4TH	54.04608	.08805	.26615	.53416	1.00000
		5TH	79.71292	.05970	.18043	.36310	.60642 1.00000

TABLE 1. NATURAL FREQUENCIES AND NODES FOR TAPERED CANTILEVER BEAMS

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.50	.10	1ST	5.48156	1.00000			
		2ND	25.80637	.28400	1.00000		
		3RD	64.76696	.17751	.51944	1.00000	
		4TH	121.46787	.12741	.37437	.64696	1.00000
		5TH	195.99795	.09905	.29098	.50395	.72107 1.00000
.50	.20	1ST	5.70617	1.00000			
		2ND	25.09250	.28752	1.00000		
		3RD	61.09063	.17768	.51321	1.00000	
		4TH	113.03085	.12616	.36590	.63806	1.00000
		5TH	180.97245	.09713	.28166	.49227	.71220 1.00000
.50	.30	1ST	5.91792	1.00000			
		2ND	24.33867	.29001	1.00000		
		3RD	57.48205	.17701	.50638	1.00000	
		4TH	104.85989	.12422	.35682	.62858	1.00000
		5TH	166.50990	.09464	.27179	.47990	.70268 1.00000
.50	.40	1ST	6.11574	1.00000			
		2ND	23.54703	.29149	1.00000		
		3RD	53.94163	.17549	.49889	1.00000	
		4TH	96.95525	.12159	.34707	.61844	1.00000
		5TH	152.61052	.09157	.26134	.46679	.69244 1.00000
.50	.50	1ST	6.29851	1.00000			
		2ND	22.71946	.29195	1.00000		
		3RD	50.46977	.17314	.49068	1.00000	
		4TH	89.31721	.11829	.33659	.60756	1.00000
		5TH	139.27439	.08797	.25027	.45285	.68139 1.00000
.50	.60	1ST	6.46495	1.00000			
		2ND	21.85763	.29137	1.00000		
		3RD	47.06685	.16993	.48168	1.00000	
		4TH	81.94603	.11431	.32533	.59585	1.00000
		5TH	126.50177	.08383	.23854	.43798	.66942 1.00000
.50	.80	1ST	6.74316	1.00000			
		2ND	20.03664	.28694	1.00000		
		3RD	40.46916	.16082	.46089	1.00000	
		4TH	68.00520	.10432	.30012	.56942	1.00000
		5TH	102.64750	.07402	.21293	.40503	.64215 1.00000
.50	1.00	1ST	6.93705	1.00000			
		2ND	18.09205	.27760	1.00000		
		3RD	34.15046	.14784	.43545	1.00000	
		4TH	55.13427	.09155	.27065	.53784	1.00000
		5TH	81.04880	.06228	.18408	.36679	.60915 1.00000

TABLE 1. NATURAL FREQUENCIES AND NODES FOR TAPERED CANTILEVER BEAMS

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.60	.10	1ST	5.84844	1.00000			
		2ND	26.67514	.29418	1.00000		
		3RD	66.09489	.18496	.52450	1.00000	
		4TH	123.26350	.13316	.37911	.64959	1.00000
		5TH	198.26140	.10369	.29516	.50684	.72269
.60	.20	1ST	6.07203	1.00000			
		2ND	25.92884	.29719	1.00000		
		3RD	62.36461	.18477	.51822	1.00000	
		4TH	114.74832	.13160	.37060	.64077	1.00000
		5TH	183.13340	.10150	.28579	.49523	.71390
.60	.30	1ST	6.28241	1.00000			
		2ND	25.14344	.29922	1.00000		
		3RD	58.70225	.18375	.51135	1.00000	
		4TH	106.49930	.12937	.36147	.63138	1.00000
		5TH	168.56846	.09875	.27586	.48294	.70447
.60	.40	1ST	6.47850	1.00000			
		2ND	24.32092	.30028	1.00000		
		3RD	55.10819	.18192	.50384	1.00000	
		4TH	98.51672	.12647	.35168	.62133	1.00000
		5TH	154.56667	.09545	.26535	.46991	.69432
.60	.50	1ST	6.65916	1.00000			
		2ND	23.46308	.30036	1.00000		
		3RD	51.58284	.17928	.49562	1.00000	
		4TH	90.80081	.12292	.34117	.61055	1.00000
		5TH	141.12825	.09161	.25422	.45605	.68338
.60	.60	1ST	6.82309	1.00000			
		2ND	22.57145	.29944	1.00000		
		3RD	48.12654	.17579	.48661	1.00000	
		4TH	83.35184	.11870	.32987	.59894	1.00000
		5TH	128.25335	.08725	.24244	.44126	.67152
.60	.80	1ST	7.09501	1.00000			
		2ND	20.69188	.29441	1.00000		
		3RD	41.42238	.16618	.46584	1.00000	
		4TH	69.25565	.10825	.30461	.57274	1.00000
		5TH	104.19474	.07702	.21669	.40848	.64451
.60	1.00	1ST	7.28073	1.00000			
		2ND	18.68930	.28455	1.00000		
		3RD	34.99732	.15271	.44046	1.00000	
		4TH	56.22945	.09503	.27506	.54143	1.00000
		5TH	82.39172	.06486	.18769	.37042	.61182

TABLE 1. NATURAL FREQUENCIES AND NODES FOR TAPERED CANTILEVER BEAMS

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.80	.10	1ST	6.60401	1.00000			
		2ND	28.42930	.31329	1.00000		
		3RD	68.77063	.19919	.53411	1.00000	
		4TH	126.87519	.14423	.38822	.65467	1.00000
		5TH	202.80911	.11268	.30325	.51246	.72585 1.00000
.80	.20	1ST	6.82529	1.00000			
		2ND	27.61914	.31539	1.00000		
		3RD	64.93265	.19833	.52777	1.00000	
		4TH	118.20383	.14211	.37963	.64601	1.00000
		5TH	187.47620	.10999	.29377	.50099	.71721 1.00000
.80	.30	1ST	7.03265	1.00000			
		2ND	26.77137	.31660	1.00000		
		3RD	61.16289	.19670	.52086	1.00000	
		4TH	109.79881	.13936	.37043	.63679	1.00000
		5TH	172.70647	.10676	.28375	.48885	.70795 1.00000
.80	.40	1ST	7.22499	1.00000			
		2ND	25.88775	.31693	1.00000		
		3RD	57.46172	.19430	.51331	1.00000	
		4TH	101.66040	.13597	.36058	.62692	1.00000
		5TH	158.50002	.10302	.27314	.47598	.69799 1.00000
.80	.50	1ST	7.40113	1.00000			
		2ND	24.96983	.31634	1.00000		
		3RD	53.82950	.19113	.50508	1.00000	
		4TH	93.78885	.13195	.35002	.61633	1.00000
		5TH	144.85704	.09875	.26192	.46227	.68724 1.00000
.80	.60	1ST	7.55975	1.00000			
		2ND	24.01897	.31481	1.00000		
		3RD	50.26657	.18714	.49608	1.00000	
		4TH	86.18438	.12729	.33867	.60492	1.00000
		5TH	131.77768	.09399	.25003	.44766	.67560 1.00000
.80	.80	1ST	7.81849	1.00000			
		2ND	22.02259	.30869	1.00000		
		3RD	43.34957	.17660	.47537	1.00000	
		4TH	71.77754	.11598	.31331	.57918	1.00000
		5TH	107.31037	.08296	.22406	.41522	.64909 1.00000
.80	1.00	1ST	7.98725	1.00000			
		2ND	19.90401	.29790	1.00000		
		3RD	36.71176	.16225	.45011	1.00000	
		4TH	58.44082	.10190	.28364	.54839	1.00000
		5TH	85.09876	.06998	.19476	.37750	.61700 1.00000

TABLE 1. NATURAL FREQUENCIES AND NODES FOR TAPERED CANTILEVER BEAMS

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
1.00	.10	1ST	7.38863	1.00000			
		2ND	30.20649	.33090	1.00000		
		3RD	71.47303	.21260	.54313	1.00000	
		4TH	130.51427	.15477	.39688	.65954	1.00000
		5TH	207.38463	.12130	.31099	.51788	.72891
1.00	.20	1ST	7.60720	1.00000			
		2ND	29.33359	.33224	1.00000		
		3RD	67.52760	.21115	.53675	1.00000	
		4TH	121.68684	.15216	.38823	.65104	1.00000
		5TH	191.84694	.11816	.30143	.50655	.72042
1.00	.30	1ST	7.81115	1.00000			
		2ND	28.42435	.33276	1.00000		
		3RD	63.65066	.20899	.52981	1.00000	
		4TH	113.12596	.14895	.37898	.64197	1.00000
		5TH	176.87248	.11451	.29133	.49456	.71132
1.00	.40	1ST	7.99934	1.00000			
		2ND	27.48032	.33246	1.00000		
		3RD	59.84256	.20610	.52226	1.00000	
		4TH	104.83184	.14512	.36909	.63227	1.00000
		5TH	162.46145	.11036	.28064	.48183	.70154
1.00	.50	1ST	8.17056	1.00000			
		2ND	26.50287	.33129	1.00000		
		3RD	56.10363	.20245	.51403	1.00000	
		4TH	96.80474	.14068	.35849	.62186	1.00000
		5TH	148.61396	.10572	.26934	.46828	.69098
1.00	.60	1ST	8.32347	1.00000			
		2ND	25.49314	.32923	1.00000		
		3RD	52.43416	.19803	.50505	1.00000	
		4TH	89.04486	.13562	.34711	.61065	1.00000
		5TH	135.33020	.10057	.25737	.45383	.67955
1.00	.80	1ST	8.56825	1.00000			
		2ND	23.38030	.32219	1.00000		
		3RD	45.30443	.18666	.48442	1.00000	
		4TH	74.32746	.12353	.32168	.58534	1.00000
		5TH	110.45425	.08880	.23121	.42172	.65351
1.00	1.00	1ST	8.71926	1.00000			
		2ND	21.14566	.31058	1.00000		
		3RD	38.45377	.17150	.45930	1.00000	
		4TH	60.68014	.10866	.29193	.55506	1.00000
		5TH	87.83399	.07507	.20166	.38434	.62200

TABLE 2. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF
ANTISYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.10	.00	1ST	16.04270	.2810	1.0000		
		2ND	51.07784	.1575	.5604	1.0000	
		3RD	105.85465	.1094	.3892	.6954	1.0000
		4TH	180.37029	.0838	.2982	.5327	.7665 1.0000
		5TH	274.62509	.0679	.2417	.4317	.6211 .8107 1.0000
.20	.00	1ST	16.67084	.2969	1.0000		
		2ND	52.19662	.1676	.5669	1.0000	
		3RD	107.46787	.1168	.3950	.6984	1.0000
		4TH	182.47738	.0897	.3032	.5359	.7682 1.0000
		5TH	277.22591	.0727	.2460	.4348	.6232 .8118 1.0000
.30	.00	1ST	17.30292	.3118	1.0000		
		2ND	53.32124	.1774	.5732	1.0000	
		3RD	109.08740	.1240	.4007	.7013	1.0000
		4TH	184.59102	.0953	.3080	.5390	.7699 1.0000
		5TH	279.83343	.0774	.2502	.4378	.6252 .8129 1.0000
.40	.00	1ST	17.93916	.3260	1.0000		
		2ND	54.45176	.1867	.5793	1.0000	
		3RD	110.71325	.1310	.4061	.7041	1.0000
		4TH	186.71124	.1009	.3127	.5421	.7715 1.0000
		5TH	282.44766	.0820	.2543	.4408	.6272 .8140 1.0000
.50	.00	1ST	18.57977	.3395	1.0000		
		2ND	55.58823	.1958	.5851	1.0000	
		3RD	112.34544	.1377	.4114	.7068	1.0000
		4TH	188.83803	.1062	.3173	.5451	.7731 1.0000
		5TH	285.06863	.0865	.2583	.4437	.6292 .8150 1.0000
.60	.00	1ST	19.22493	.3523	1.0000		
		2ND	56.73065	.2045	.5907	1.0000	
		3RD	113.98401	.1443	.4165	.7095	1.0000
		4TH	190.97142	.1114	.3218	.5481	.7747 1.0000
		5TH	287.69633	.0908	.2622	.4465	.6311 .8161 1.0000
.80	.00	1ST	20.52951	.3762	1.0000		
		2ND	59.03360	.2210	.6013	1.0000	
		3RD	117.28031	.1568	.4263	.7147	1.0000
		4TH	195.25801	.1215	.3304	.5538	.7778 1.0000
		5TH	292.97194	.0992	.2698	.4521	.6349 .8182 1.0000
1.00	.00	1ST	21.85396	.3980	1.0000		
		2ND	61.36083	.2365	.6112	1.0000	
		3RD	120.60229	.1687	.4357	.7197	1.0000
		4TH	199.57111	.1311	.3387	.5593	.7809 1.0000
		5TH	298.27457	.1073	.2770	.4575	.6386 .8202 1.0000

TABLE 2. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF
ANTISYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)				
.00	.10	1ST	15.08138	.2770	1.0000			
		2ND	47.18989	.1518	.5507	1.0000		
		3RD	97.11908	.1038	.3766	.6855	1.0000	
		4TH	164.86205	.0786	.2850	.5188	.7577	1.0000
		5TH	250.41947	.0631	.2287	.4164	.6081	.8030
.00	.20	1ST	14.71346	.2884	1.0000			
		2ND	44.46738	.1556	.5474	1.0000		
		3RD	90.21738	.1050	.3693	.6783	1.0000	
		4TH	151.95371	.0786	.2765	.5076	.7503	1.0000
		5TH	229.67805	.0625	.2198	.4035	.5964	.7960
.00	.30	1ST	14.31692	.2984	1.0000			
		2ND	41.79778	.1583	.5436	1.0000		
		3RD	83.54284	.1053	.3615	.6706	1.0000	
		4TH	139.54486	.0779	.2673	.4958	.7423	1.0000
		5TH	209.80682	.0613	.2103	.3900	.5839	.7885
.00	.40	1ST	13.89400	.3074	1.0000			
		2ND	39.18153	.1599	.5393	1.0000		
		3RD	77.09574	.1048	.3530	.6624	1.0000	
		4TH	127.63570	.0764	.2576	.4832	.7338	1.0000
		5TH	190.80585	.0595	.2003	.3759	.5707	.7804
.00	.50	1ST	13.44673	.3152	1.0000			
		2ND	36.61912	.1606	.5345	1.0000		
		3RD	70.87632	.1034	.3437	.6538	1.0000	
		4TH	116.22631	.0744	.2472	.4699	.7247	1.0000
		5TH	172.67526	.0571	.1899	.3609	.5564	.7716
.00	.60	1ST	12.97695	.3221	1.0000			
		2ND	34.11102	.1602	.5292	1.0000		
		3RD	64.88489	.1012	.3338	.6445	1.0000	
		4TH	105.31692	.0716	.2362	.4557	.7148	1.0000
		5TH	155.41518	.0542	.1789	.3451	.5412	.7621
.00	.80	1ST	11.97619	.3332	1.0000			
		2ND	29.25974	.1566	.5167	1.0000		
		3RD	53.58713	.0946	.3113	.6239	1.0000	
		4TH	84.99889	.0644	.2119	.4243	.6926	1.0000
		5TH	123.50709	.0472	.1552	.3108	.5070	.7403
.00	1.00	1ST	10.90236	.3410	1.0000			
		2ND	24.63138	.1490	.5014	1.0000		
		3RD	43.20475	.0850	.2848	.6000	1.0000	
		4TH	66.68312	.0550	.1845	.3880	.6662	1.0000
		5TH	95.08264	.0386	.1294	.2721	.4667	.7138

TABLE 2. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF
ANTISYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.10	.10	1ST	15.68218	.2928	1.0000		
		2ND	48.25902	.1618	.5574	1.0000	
		3RD	98.65841	.1110	.3825	.6886	1.0000
		4TH	166.87082	.0842	.2901	.5222	.7596 1.0000
		5TH	252.89746	.0677	.2331	.4196	.6102 .8042 1.0000
.10	.20	1ST	15.29172	.3032	1.0000		
		2ND	45.49287	.1649	.5540	1.0000	
		3RD	91.68921	.1118	.3752	.6815	1.0000
		4TH	153.87080	.0838	.2814	.5111	.7522 1.0000
		5TH	232.03995	.0667	.2240	.4068	.5987 .7973 1.0000
.10	.30	1ST	14.87364	.3125	1.0000		
		2ND	42.77983	.1671	.5502	1.0000	
		3RD	84.94729	.1116	.3672	.6740	1.0000
		4TH	141.37030	.0827	.2722	.4993	.7444 1.0000
		5TH	212.05267	.0652	.2144	.3934	.5863 .7899 1.0000
.10	.40	1ST	14.43004	.3207	1.0000		
		2ND	40.12034	.1683	.5459	1.0000	
		3RD	78.43290	.1107	.3587	.6659	1.0000
		4TH	129.36955	.0810	.2623	.4869	.7360 1.0000
		5TH	192.93569	.0631	.2044	.3793	.5732 .7819 1.0000
.10	.50	1ST	13.96281	.3280	1.0000		
		2ND	37.51488	.1685	.5410	1.0000	
		3RD	72.14631	.1090	.3494	.6574	1.0000
		4TH	117.86867	.0786	.2519	.4737	.7270 1.0000
		5TH	174.68916	.0604	.1938	.3644	.5591 .7732 1.0000
.10	.60	1ST	13.47367	.3343	1.0000		
		2ND	34.95393	.1678	.5357	1.0000	
		3RD	66.08781	.1065	.3394	.6483	1.0000
		4TH	106.86784	.0756	.2408	.4596	.7173 1.0000
		5TH	157.31317	.0573	.1827	.3487	.5440 .7638 1.0000
.10	.80	1ST	12.43560	.3446	1.0000		
		2ND	30.02742	.1635	.5233	1.0000	
		3RD	54.65624	.0993	.3168	.6280	1.0000
		4TH	86.36714	.0678	.2164	.4284	.6954 1.0000
		5TH	125.17338	.0498	.1588	.3145	.5101 .7422 1.0000
.10	1.00	1ST	11.32564	.3517	1.0000		
		2ND	25.31434	.1553	.5081	1.0000	
		3RD	44.14037	.0891	.2903	.6044	1.0000
		4TH	67.86891	.0579	.1888	.3924	.6694 1.0000
		5TH	96.51744	.0407	.1328	.2759	.4702 .7161 1.0000

TABLE 2. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF
ANTISYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.20	.10	1ST	16.28719	.3077	1.0000		
		2ND	49.33404	.1713	.5639	1.0000	
		3RD	100.20407	.1180	.3882	.6917	1.0000
		4TH	168.88618	.0896	.2950	.5255	.7614 1.0000
		5TH	255.38217	.0721	.2373	.4227	.6124 .8054 1.0000
.20	.20	1ST	15.87465	.3173	1.0000		
		2ND	46.52435	.1739	.5604	1.0000	
		3RD	93.16742	.1183	.3808	.6847	1.0000
		4TH	155.79447	.0889	.2862	.5144	.7541 1.0000
		5TH	234.40858	.0708	.2281	.4100	.6009 .7986 1.0000
.20	.30	1ST	15.43540	.3259	1.0000		
		2ND	43.75795	.1756	.5565	1.0000	
		3RD	86.35815	.1178	.3728	.6772	1.0000
		4TH	143.20236	.0875	.2769	.5028	.7464 1.0000
		5TH	214.30526	.0690	.2184	.3966	.5887 .7912 1.0000
.20	.40	1ST	14.97140	.3335	1.0000		
		2ND	41.06531	.1764	.5522	1.0000	
		3RD	79.77653	.1165	.3642	.6693	1.0000
		4TH	131.11007	.0854	.2670	.4904	.7381 1.0000
		5TH	195.07231	.0666	.2083	.3826	.5757 .7833 1.0000
.20	.50	1ST	14.48444	.3402	1.0000		
		2ND	38.41688	.1762	.5473	1.0000	
		3RD	73.42282	.1144	.3549	.6609	1.0000
		4TH	119.51771	.0827	.2565	.4773	.7292 1.0000
		5TH	176.70983	.0637	.1976	.3678	.5617 .7748 1.0000
.20	.60	1ST	13.97613	.3461	1.0000		
		2ND	35.82312	.1752	.5420	1.0000	
		3RD	67.29729	.1117	.3448	.6519	1.0000
		4TH	108.42548	.0794	.2453	.4634	.7197 1.0000
		5TH	159.21796	.0604	.1864	.3522	.5467 .7655 1.0000
.20	.80	1ST	12.90096	.3555	1.0000		
		2ND	30.80149	.1703	.5296	1.0000	
		3RD	55.73196	.1039	.3222	.6320	1.0000
		4TH	87.74213	.0712	.2208	.4324	.6981 1.0000
		5TH	126.84654	.0524	.1624	.3181	.5131 .7442 1.0000
.20	1.00	1ST	11.75495	.3620	1.0000		
		2ND	26.00374	.1615	.5146	1.0000	
		3RD	45.08263	.0932	.2956	.6088	1.0000
		4TH	69.06147	.0608	.1930	.3966	.6725 1.0000
		5TH	97.95907	.0429	.1361	.2796	.4736 .7184 1.0000

TABLE 2. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF
ANTISYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.30	.10	1ST	16.89661	.3218	1.0000		
		2ND	50.41502	.1805	.5701	1.0000	
		3RD	101.75608	.1247	.3938	.6947	1.0000
		4TH	170.90811	.0949	.2997	.5287	.7631 1.0000
		5TH	257.87359	.0765	.2414	.4258	.6145 .8066 1.0000
.30	.20	1ST	16.46240	.3307	1.0000		
		2ND	47.56186	.1827	.5666	1.0000	
		3RD	94.65202	.1246	.3863	.6878	1.0000
		4TH	157.72475	.0938	.2909	.5177	.7560 1.0000
		5TH	236.78396	.0749	.2321	.4131	.6031 .7998 1.0000
.30	.30	1ST	16.00231	.3386	1.0000		
		2ND	44.75219	.1839	.5626	1.0000	
		3RD	87.77546	.1238	.3783	.6804	1.0000
		4TH	145.04106	.0921	.2815	.5062	.7484 1.0000
		5TH	216.56462	.0728	.2224	.3999	.5910 .7926 1.0000
.30	.40	1ST	15.51818	.3457	1.0000		
		2ND	42.01646	.1843	.5583	1.0000	
		3RD	81.12665	.1222	.3696	.6726	1.0000
		4TH	132.85724	.0897	.2716	.4939	.7402 1.0000
		5TH	197.21571	.0701	.2121	.3859	.5781 .7847 1.0000
.30	.50	1ST	15.01169	.3519	1.0000		
		2ND	39.32513	.1838	.5534	1.0000	
		3RD	74.70584	.1198	.3603	.6643	1.0000
		4TH	121.17343	.0868	.2610	.4809	.7314 1.0000
		5TH	178.73730	.0670	.2014	.3712	.5643 .7763 1.0000
.30	.60	1ST	14.48436	.3573	1.0000		
		2ND	36.68863	.1824	.5481	1.0000	
		3RD	68.51333	.1168	.3502	.6555	1.0000
		4TH	109.98981	.0833	.2497	.4671	.7220 1.0000
		5TH	161.12957	.0634	.1901	.3556	.5494 .7671 1.0000
.30	.80	1ST	13.37229	.3660	1.0000		
		2ND	31.58196	.1769	.5358	1.0000	
		3RD	56.81429	.1085	.3275	.6359	1.0000
		4TH	89.12387	.0745	.2251	.4364	.7008 1.0000
		5TH	128.52653	.0549	.1659	.3216	.5161 .7461 1.0000
.30	1.00	1ST	12.19031	.3719	1.0000		
		2ND	26.69958	.1676	.5209	1.0000	
		3RD	46.03153	.0972	.3009	.6130	1.0000
		4TH	70.26080	.0637	.1972	.4008	.6755 1.0000
		5TH	99.40757	.0450	.1393	.2833	.4769 .7207 1.0000

TABLE 2. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF
ANTISYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)				
.40	.10	1ST	17.51065	.3352	1.0000			
		2ND	51.50197	.1894	.5761	1.0000		
		3RD	103.31447	.1313	.3992	.6976	1.0000	
		4TH	172.93664	.1001	.3044	.5318	.7649	1.0000
		5TH	260.37175	.0807	.2454	.4288	.6166	.8077 1.0000
.40	.20	1ST	17.05512	.3434	1.0000			
		2ND	48.60544	.1911	.5725	1.0000		
		3RD	96.14306	.1308	.3916	.6908	1.0000	
		4TH	159.66165	.0987	.2955	.5210	.7578	1.0000
		5TH	239.16609	.0788	.2361	.4162	.6053	.8011 1.0000
.40	.30	1ST	16.57447	.3508	1.0000			
		2ND	45.76257	.1919	.5685	1.0000		
		3RD	89.19922	.1296	.3836	.6835	1.0000	
		4TH	146.88642	.0967	.2860	.5095	.7503	1.0000
		5TH	218.83077	.0765	.2262	.4030	.5933	.7939 1.0000
.40	.40	1ST	16.07045	.3573	1.0000			
		2ND	42.97383	.1919	.5641	1.0000		
		3RD	82.48326	.1277	.3749	.6759	1.0000	
		4TH	134.61109	.0940	.2760	.4974	.7422	1.0000
		5TH	199.36589	.0736	.2159	.3891	.5805	.7861 1.0000
.40	.50	1ST	15.54461	.3631	1.0000			
		2ND	40.23965	.1911	.5593	1.0000		
		3RD	75.99541	.1251	.3655	.6677	1.0000	
		4TH	122.83585	.0908	.2654	.4845	.7336	1.0000
		5TH	180.77160	.0702	.2051	.3745	.5668	.7778 1.0000
.40	.60	1ST	14.99840	.3681	1.0000			
		2ND	37.56047	.1894	.5540	1.0000		
		3RD	69.73595	.1218	.3554	.6590	1.0000	
		4TH	111.56086	.0870	.2541	.4707	.7243	1.0000
		5TH	163.04798	.0664	.1938	.3590	.5521	.7687 1.0000
.40	.80	1ST	13.84960	.3762	1.0000			
		2ND	32.36883	.1834	.5418	1.0000		
		3RD	57.90325	.1130	.3327	.6397	1.0000	
		4TH	90.51236	.0779	.2293	.4402	.7033	1.0000
		5TH	130.21336	.0575	.1694	.3252	.5191	.7480 1.0000
.40	1.00	1ST	12.63170	.3816	1.0000			
		2ND	27.40185	.1736	.5271	1.0000		
		3RD	46.98707	.1013	.3061	.6172	1.0000	
		4TH	71.46690	.0666	.2012	.4049	.6785	1.0000
		5TH	100.86293	.0472	.1426	.2869	.4802	.7229 1.0000

TABLE 2. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF
ANTISYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.50	.10	1ST	18.12946	.3480	1.0000		
		2ND	52.59495	.1979	.5818	1.0000	
		3RD	104.87926	.1376	.4044	.7004	1.0000
		4TH	174.97178	.1051	.3089	.5349	.7666 1.0000
		5TH	262.87666	.0849	.2493	.4318	.6187 .8089 1.0000
.50	.20	1ST	17.65293	.3556	1.0000		
		2ND	49.65511	.1992	.5782	1.0000	
		3RD	97.64051	.1369	.3968	.6937	1.0000
		4TH	161.60520	.1034	.2999	.5242	.7596 1.0000
		5TH	241.55497	.0827	.2399	.4193	.6075 .8023 1.0000
.50	.30	1ST	17.15199	.3625	1.0000		
		2ND	46.76913	.1997	.5742	1.0000	
		3RD	90.62948	.1353	.3887	.6866	1.0000
		4TH	148.73843	.1011	.2905	.5128	.7522 1.0000
		5TH	221.10368	.0801	.2300	.4061	.5956 .7952 1.0000
.50	.40	1ST	16.62827	.3685	1.0000		
		2ND	43.93743	.1994	.5698	1.0000	
		3RD	83.84638	.1331	.3800	.6790	1.0000
		4TH	136.37164	.0982	.2804	.5007	.7442 1.0000
		5TH	201.52288	.0770	.2197	.3923	.5829 .7875 1.0000
.50	.50	1ST	16.08326	.3739	1.0000		
		2ND	41.16046	.1982	.5650	1.0000	
		3RD	77.29152	.1303	.3706	.6710	1.0000
		4TH	124.50496	.0948	.2697	.4879	.7357 1.0000
		5TH	182.81269	.0734	.2088	.3777	.5693 .7793 1.0000
.50	.60	1ST	15.51829	.3786	1.0000		
		2ND	38.43865	.1963	.5597	1.0000	
		3RD	70.96514	.1267	.3605	.6624	1.0000
		4TH	113.13864	.0908	.2583	.4743	.7265 1.0000
		5TH	164.97322	.0693	.1973	.3623	.5547 .7703 1.0000
.50	.80	1ST	14.33292	.3860	1.0000		
		2ND	33.16211	.1898	.5476	1.0000	
		3RD	58.99883	.1174	.3378	.6434	1.0000
		4TH	91.90761	.0812	.2335	.4440	.7059 1.0000
		5TH	131.90701	.0601	.1728	.3286	.5219 .7499 1.0000
.50	1.00	1ST	13.07914	.3909	1.0000		
		2ND	28.11056	.1795	.5330	1.0000	
		3RD	47.94925	.1053	.3111	.6212	1.0000
		4TH	72.67976	.0695	.2053	.4090	.6814 1.0000
		5TH	102.32514	.0493	.1458	.2905	.4834 .7251 1.0000

TABLE 2. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF
ANTISYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)		
.60	.10	1ST	18.75316	.3602	1.0000	
		2ND	53.69398	.2062	.5874	1.0000
		3RD	106.45044	.1438	.4095	.7032 1.0000
		4TH	177.01355	.1101	.3133	.5379 .7683 1.0000
		5TH	265.38832	.0889	.2532	.4347 .6207 .8100 1.0000
.60	.20	1ST	18.25593	.3673	1.0000	
		2ND	50.71092	.2071	.5838	1.0000
		3RD	99.14442	.1427	.4019	.6966 1.0000
		4TH	163.55538	.1081	.3043	.5273 .7614 1.0000
		5TH	243.95063	.0866	.2437	.4223 .6096 .8035 1.0000
.60	.30	1ST	17.73493	.3736	1.0000	
		2ND	47.78188	.2073	.5797	1.0000
		3RD	92.06621	.1409	.3937	.6896 1.0000
		4TH	150.59710	.1055	.2948	.5160 .7540 1.0000
		5TH	223.38338	.0837	.2338	.4092 .5978 .7964 1.0000
.60	.40	1ST	17.19172	.3793	1.0000	
		2ND	44.90730	.2066	.5753	1.0000
		3RD	85.21605	.1385	.3850	.6821 1.0000
		4TH	138.13886	.1024	.2847	.5040 .7462 1.0000
		5TH	203.68665	.0803	.2233	.3954 .5852 .7889 1.0000
.60	.50	1ST	16.62768	.3843	1.0000	
		2ND	42.08759	.2052	.5705	1.0000
		3RD	78.59420	.1353	.3756	.6742 1.0000
		4TH	126.18083	.0987	.2739	.4913 .7378 1.0000
		5TH	184.86059	.0765	.2124	.3809 .5717 .7807 1.0000
.60	.60	1ST	16.04405	.3886	1.0000	
		2ND	39.32319	.2030	.5652	1.0000
		3RD	72.20091	.1315	.3654	.6657 1.0000
		4TH	114.72316	.0945	.2625	.4778 .7287 1.0000
		5TH	166.90530	.0723	.2009	.3655 .5572 .7719 1.0000
.60	.80	1ST	14.82223	.3955	1.0000	
		2ND	33.95182	.1960	.5532	1.0000
		3RD	60.10104	.1218	.3427	.6470 1.0000
		4TH	93.30962	.0844	.2376	.4478 .7084 1.0000
		5TH	133.60754	.0626	.1761	.3320 .5248 .7517 1.0000
.60	1.00	1ST	13.53261	.4000	1.0000	
		2ND	28.82571	.1853	.5388	1.0000
		3RD	48.91807	.1092	.3161	.6252 1.0000
		4TH	73.89939	.0723	.2093	.4129 .6843 1.0000
		5TH	103.79419	.0515	.1490	.2940 .4865 .7273 1.0000

TABLE 2. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF
ANTISYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)				
.80	.10	1ST	20.01576	.3830	1.0000			
		2ND	55.91034	.2220	.5979	1.0000		
		3RD	109.61211	.1558	.4192	.7086	1.0000	
		4TH	181.11694	.1196	.3219	.5438	.7715	1.0000
		5TH	270.43190	.0968	.2606	.4404	.6247	.8122 1.0000
.80	.20	1ST	19.47788	.3892	1.0000			
		2ND	52.84103	.2222	.5943	1.0000		
		3RD	102.17166	.1541	.4116	.7021	1.0000	
		4TH	167.47572	.1171	.3128	.5333	.7648	1.0000
		5TH	248.76226	.0940	.2511	.4281	.6138	.8058 1.0000
.80	.30	1ST	18.91740	.3947	1.0000			
		2ND	49.82607	.2218	.5902	1.0000		
		3RD	94.95921	.1518	.4034	.6953	1.0000	
		4TH	154.33448	.1141	.3032	.5222	.7577	1.0000
		5TH	227.96313	.0907	.2410	.4152	.6021	.7989 1.0000
.80	.40	1ST	18.33567	.3996	1.0000			
		2ND	46.86588	.2206	.5859	1.0000		
		3RD	87.97500	.1488	.3946	.6881	1.0000	
		4TH	141.69343	.1105	.2930	.5105	.7500	1.0000
		5TH	208.03464	.0869	.2304	.4015	.5898	.7915 1.0000
.80	.50	1ST	17.73395	.4039	1.0000			
		2ND	43.96086	.2186	.5811	1.0000		
		3RD	81.21926	.1452	.3852	.6803	1.0000	
		4TH	129.55267	.1064	.2822	.4979	.7418	1.0000
		5TH	188.97685	.0827	.2194	.3872	.5765	.7836 1.0000
.80	.60	1ST	17.11332	.4076	1.0000			
		2ND	41.11139	.2159	.5759	1.0000		
		3RD	74.69226	.1410	.3750	.6721	1.0000	
		4TH	117.91239	.1018	.2707	.4846	.7330	1.0000
		5TH	170.78995	.0781	.2078	.3719	.5623	.7749 1.0000
.80	.80	1ST	15.81892	.4135	1.0000			
		2ND	35.58051	.2081	.5640	1.0000		
		3RD	62.32536	.1305	.3524	.6539	1.0000	
		4TH	96.13392	.0909	.2456	.4550	.7132	1.0000
		5TH	137.02913	.0677	.1828	.3387	.5303	.7552 1.0000
.80	1.00	1ST	14.45767	.4172	1.0000			
		2ND	30.27530	.1967	.5499	1.0000		
		3RD	50.87562	.1171	.3257	.6328	1.0000	
		4TH	76.35894	.0780	.2171	.4206	.6898	1.0000
		5TH	106.75287	.0558	.1553	.3009	.4927	.7315 1.0000

TABLE 2. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF
ANTISYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)		
1.00	.10	1ST	21.29928	.4040	1.0000	
		2ND	58.15127	.2368	.6078	1.0000
		3RD	112.79963	.1671	.4285	.7137 1.0000
		4TH	185.24694	.1287	.3300	.5495 .7747 1.0000
		5TH	275.50256	.1045	.2678	.4459 .6285 .8143 1.0000
1.00	.20	1ST	20.72162	.4093	1.0000	
		2ND	54.99597	.2365	.6041	1.0000
		3RD	105.22490	.1650	.4208	.7075 1.0000
		4TH	171.42275	.1258	.3209	.5392 .7681 1.0000
		5TH	253.60104	.1012	.2581	.4338 .6178 .8081 1.0000
1.00	.30	1ST	20.12233	.4141	1.0000	
		2ND	51.89532	.2355	.6001	1.0000
		3RD	97.87833	.1622	.4126	.7098 1.0000
		4TH	158.09865	.1223	.3112	.5282 .7612 1.0000
		5TH	232.57011	.0975	.2480	.4210 .6064 .8013 1.0000
1.00	.40	1ST	19.50265	.4184	1.0000	
		2ND	48.84971	.2338	.5958	1.0000
		3RD	90.76018	.1588	.4038	.6937 1.0000
		4TH	145.27482	.1184	.3010	.5166 .7537 1.0000
		5TH	212.40985	.0933	.2374	.4075 .5942 .7941 1.0000
1.00	.50	1ST	18.86367	.4221	1.0000	
		2ND	45.85953	.2315	.5910	1.0000
		3RD	83.87066	.1548	.3944	.6863 1.0000
		4TH	132.95142	.1139	.2901	.5043 .7457 1.0000
		5TH	193.12044	.0888	.2262	.3932 .5811 .7863 1.0000
1.00	.60	1ST	18.20635	.4254	1.0000	
		2ND	42.92513	.2283	.5859	1.0000
		3RD	77.21004	.1502	.3843	.6783 1.0000
		4TH	121.12860	.1089	.2786	.4912 .7371 1.0000
		5TH	174.70194	.0838	.2145	.3781 .5671 .7779 1.0000
1.00	.80	1ST	16.83970	.4304	1.0000	
		2ND	37.22491	.2198	.5742	1.0000
		3RD	64.57622	.1389	.3616	.6606 1.0000
		4TH	98.98528	.0973	.2533	.4620 .7179 1.0000
		5TH	140.47814	.0727	.1892	.3451 .5357 .7587 1.0000
1.00	1.00	1ST	15.40683	.4334	1.0000	
		2ND	31.75062	.2076	.5604	1.0000
		3RD	52.85972	.1247	.3350	.6400 1.0000
		4TH	78.84556	.0836	.2246	.4281 .6951 1.0000
		5TH	109.73896	.0601	.1614	.3076 .4987 .7355 1.0000

TABLE 3. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF SYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.10	.00	1ST	5.96531	.46975			
		2ND	31.09310	.20187	.71811		
		3RD	75.99965	.12912	.45938	.82068	
		4TH	140.64556	.09492	.33769	.60327	.86795
		5TH	225.03065	.07504	.26696	.47693	.68618 .89554
.20	.00	1ST	6.34515	.48935			
		2ND	31.96779	.21423	.72426		
		3RD	77.35779	.13770	.46560	.82303	
		4TH	142.50713	.10146	.34306	.60642	.86922
		5TH	227.38572	.08032	.27159	.48008	.68812 .89532
.30	.00	1ST	6.73274	.50735			
		2ND	32.84992	.22601	.73009		
		3RD	78.74329	.14597	.47159	.82531	
		4TH	144.37609	.10780	.34828	.60950	.87045
		5TH	229.74813	.08546	.27609	.48317	.69003 .89709
.40	.00	1ST	7.12804	.52396			
		2ND	33.73947	.23726	.73562		
		3RD	80.12618	.15395	.47738	.82753	
		4TH	146.25239	.11395	.35335	.61251	.87166
		5TH	232.11789	.09045	.28048	.48620	.69190 .89785
.50	.00	1ST	7.53098	.53933			
		2ND	34.63642	.24802	.74089		
		3RD	81.51643	.16167	.48297	.82968	
		4TH	148.13605	.11993	.35827	.61546	.87284
		5TH	234.49499	.09532	.28476	.48917	.69374 .89859
.60	.00	1ST	7.94150	.55362			
		2ND	35.54077	.25834	.74591		
		3RD	82.91404	.16914	.48837	.83177	
		4TH	150.02705	.12574	.36306	.61834	.87400
		5TH	236.87944	.10007	.28893	.49209	.69555 .89933
.80	.00	1ST	8.78507	.57938			
		2ND	37.37162	.27776	.75529		
		3RD	85.73135	.18339	.49867	.83578	
		4TH	153.83114	.13691	.37227	.62392	.87624
		5TH	241.67039	.10923	.29701	.49779	.69909 .90076
1.00	.00	1ST	9.65836	.60201			
		2ND	39.23190	.29576	.76387		
		3RD	88.57805	.19683	.50835	.83957	
		4TH	157.66458	.14753	.38103	.62928	.87840
		5TH	246.49069	.11799	.30474	.50328	.70252 .90214

TABLE 3. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF SYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.00	.10	1ST	5.78131	.46626			
		2ND	28.95721	.19634	.71191		
		3RD	69.97776	.12340	.44749	.81453	
		4TH	128.81296	.08950	.32457	.59079	.86277
		5TH	205.46280	.07000	.25386	.46207	.67480 .89113
.00	.20	1ST	5.95253	.48209			
		2ND	27.69303	.20243	.71182		
		3RD	65.44420	.12554	.44146	.81058	
		4TH	119.18417	.08998	.31642	.58097	.85862
		5TH	188.91291	.06966	.24498	.44980	.66476 .88726
.00	.30	1ST	6.10602	.49608			
		2ND	26.43320	.20725	.71133		
		3RD	61.03814	.12668	.43479	.80639	
		4TH	109.90489	.08963	.30764	.57055	.85417
		5TH	173.03329	.06863	.23555	.43686	.65403 .88309
.00	.40	1ST	6.24080	.50845			
		2ND	25.17752	.21085	.71042		
		3RD	56.75954	.12686	.42743	.80191	
		4TH	100.97510	.08851	.29820	.55945	.84940
		5TH	157.82389	.06695	.22557	.42319	.64252 .87858
.00	.50	1ST	6.35582	.51939			
		2ND	23.92577	.21326	.70908		
		3RD	52.60829	.12612	.41932	.79712	
		4TH	92.39474	.08664	.28806	.54759	.84427
		5TH	143.28472	.06467	.21501	.40871	.63015 .87369
.00	.60	1ST	6.45002	.52904			
		2ND	22.67767	.21450	.70728		
		3RD	48.58426	.12447	.41040	.79198	
		4TH	84.16375	.08407	.27718	.53488	.83871
		5TH	129.41568	.06182	.20384	.39335	.61679 .86836
.00	.80	1ST	6.57120	.54491			
		2ND	20.19084	.21341	.70218		
		3RD	40.91702	.11847	.38975	.78038	
		4TH	68.74930	.07688	.25292	.50640	.82610
		5TH	103.68770	.05459	.17959	.35957	.58656 .85609
.00	1.00	1ST	6.59365	.55667			
		2ND	17.71250	.20723	.69469		
		3RD	33.75518	.10874	.36453	.76654	
		4TH	54.73005	.06707	.22482	.47277	.81089
		5TH	80.63878	.04552	.15259	.32087	.55036 .84104

TABLE 3. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF SYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)				
.10	.10	1ST	6.15072	.48586				
		2ND	29.79616	.20850	.71824			
		3RD	71.28543	.13174	.45385	.81703		
		4TH	130.58940	.09579	.33002	.59410	.86413	
		5TH	207.70799	.07503	.25850	.46536	.67686	.89198
.10	.20	1ST	6.31897	.50013				
		2ND	28.50364	.21387	.71800			
		3RD	66.69875	.13336	.44773	.81316		
		4TH	120.88277	.09584	.32177	.58439	.86005	
		5TH	191.05561	.07432	.24952	.45317	.66693	.88817
.10	.30	1ST	6.46911	.51279				
		2ND	27.21538	.21805	.71738			
		3RD	62.23955	.13404	.44099	.80905		
		4TH	111.52566	.09511	.31291	.57407	.85568	
		5TH	175.07348	.07295	.24000	.44031	.65631	.88406
.10	.40	1ST	6.60016	.52403				
		2ND	25.93119	.22107	.71637			
		3RD	57.90776	.13380	.43356	.80467		
		4TH	102.51802	.09363	.30340	.56308	.85100	
		5TH	159.76156	.07096	.22993	.42673	.64492	.87962
.10	.50	1ST	6.71110	.53398				
		2ND	24.65083	.22297	.71495			
		3RD	53.70329	.13268	.42541	.79998		
		4TH	93.85979	.09144	.29319	.55133	.84596	
		5TH	145.11982	.06839	.21927	.41234	.63267	.87480
.10	.60	1ST	6.80083	.54279				
		2ND	23.37400	.22375	.71310			
		3RD	49.62598	.13068	.41645	.79493		
		4TH	85.55088	.08857	.28224	.53874	.84051	
		5TH	131.14822	.06527	.20802	.39706	.61946	.86956
.10	.80	1ST	6.91196	.55728				
		2ND	20.82924	.22185	.70794			
		3RD	41.85190	.12403	.39576	.78359		
		4TH	69.98044	.08081	.25786	.51054	.82814	
		5TH	105.21501	.05753	.18357	.36345	.58954	.85750
.10	1.00	1ST	6.92273	.56801				
		2ND	18.29207	.21497	.70049			
		3RD	34.58267	.11370	.37051	.77005		
		4TH	55.80481	.07046	.22961	.47721	.81324	
		5TH	81.96057	.04798	.15634	.32492	.55371	.84272

TABLE 3. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF SYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.20	.10	1ST	6.52781	.50388			
		2ND	30.64254	.22011	.72424		
		3RD	72.60046	.13979	.45998	.81945	
		4TH	132.37318	.10190	.33531	.59734	.86545
		5TH	209.96057	.07994	.26303	.46858	.67889 .89282
.20	.20	1ST	6.69293	.51680			
		2ND	29.32163	.22482	.72387		
		3RD	67.96065	.14094	.45379	.81566	
		4TH	122.58873	.10155	.32698	.58773	.86144
		5TH	193.20567	.07887	.25396	.45647	.66906 .88906
.20	.30	1ST	6.83959	.52831			
		2ND	28.00492	.22841	.72314		
		3RD	63.44830	.14119	.44697	.81163	
		4TH	113.15379	.10046	.31805	.57751	.85715
		5TH	177.12101	.07718	.24435	.44370	.65854 .88501
.20	.40	1ST	6.96679	.53854			
		2ND	26.69218	.23091	.72205		
		3RD	59.06333	.14056	.43950	.80734	
		4TH	104.06828	.09866	.30847	.56662	.85255
		5TH	161.70657	.07490	.23420	.43019	.64727 .88064
.20	.50	1ST	7.07350	.54763			
		2ND	25.38318	.23234	.72056		
		3RD	54.80561	.13908	.43130	.80274	
		4TH	95.33216	.09616	.29820	.55499	.84760
		5TH	146.96230	.07206	.22346	.41589	.63515 .87589
.20	.60	1ST	7.15866	.55568			
		2ND	24.07757	.23269	.71865		
		3RD	50.67498	.13675	.42232	.79780	
		4TH	86.94532	.09300	.28719	.54252	.84225
		5TH	132.88810	.06869	.21212	.40070	.62207 .87073
.20	.80	1ST	7.25951	.56895			
		2ND	21.47475	.23005	.71345		
		3RD	42.79401	.12950	.40159	.78669	
		4TH	71.21884	.08471	.26269	.51458	.83012
		5TH	106.74961	.06046	.18749	.36726	.59246 .85887
.20	1.00	1ST	7.25837	.57875			
		2ND	18.87860	.22252	.70605		
		3RD	35.41729	.11861	.37635	.77344	
		4TH	56.88678	.07385	.23431	.48154	.81552
		5TH	83.28960	.05044	.16004	.32889	.55700 .84435

TABLE 3. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF SYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.30	.10	1ST	6.91251	.52052			
		2ND	31.49632	.23122	.72993		
		3RD	73.92286	.14757	.46590	.82181	
		4TH	134.16430	.10784	.34045	.60051	.86675
		5TH	212.22046	.08471	.26744	.47174	.68089 .89364
.30	.20	1ST	7.07437	.53226			
		2ND	30.14701	.23533	.72945		
		3RD	69.22991	.14828	.45964	.81809	
		4TH	124.30202	.10712	.33205	.59099	.86281
		5TH	195.36306	.08333	.25829	.45971	.67115 .88993
.30	.30	1ST	7.21740	.54275			
		2ND	28.80179	.23839	.72863		
		3RD	64.66439	.14814	.45277	.81413	
		4TH	114.78924	.10570	.32305	.58087	.85859
		5TH	179.17588	.08134	.24861	.44702	.66074 .88594
.30	.40	1ST	7.34061	.55210			
		2ND	27.46048	.24041	.72746		
		3RD	60.22621	.14716	.44525	.80992	
		4TH	105.62587	.10358	.31341	.57009	.85407
		5TH	163.65890	.07878	.23838	.43360	.64958 .88163
.30	.50	1ST	7.44300	.56042			
		2ND	26.12277	.24140	.72591		
		3RD	55.91522	.14535	.43703	.80542	
		4TH	96.81186	.10080	.30309	.55857	.84921
		5TH	148.81207	.07568	.22756	.41938	.63758 .87696
.30	.60	1ST	7.52346	.56780			
		2ND	24.78834	.24136	.72397		
		3RD	51.73126	.14271	.42802	.80058	
		4TH	88.34706	.09737	.29203	.54622	.84396
		5TH	134.63529	.07207	.21614	.40427	.62464 .87188
.30	.80	1ST	7.61380	.57997			
		2ND	22.12734	.23801	.71874		
		3RD	43.74332	.13488	.40727	.78969	
		4TH	72.46450	.08857	.26743	.51853	.83205
		5TH	108.29149	.06337	.19135	.37100	.59533 .86022
.30	1.00	1ST	7.60053	.58894			
		2ND	19.47208	.22988	.71139		
		3RD	36.25901	.12345	.38204	.77672	
		4TH	57.97592	.07721	.23893	.48577	.81773
		5TH	84.62586	.05290	.16369	.33280	.56022 .84595

TABLE 3. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF SYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.40	.10	1ST	7.30476	.53593			
		2ND	32.35749	.24186	.73535		
		3RD	75.25262	.15511	.47161	.82409	
		4TH	135.96279	.11361	.34544	.60361	.86802
		5TH	214.48772	.08938	.27175	.47485	.68285 .89444
.40	.20	1ST	7.46322	.54664			
		2ND	30.97974	.24542	.73477		
		3RD	70.50652	.15542	.46530	.82044	
		4TH	126.02268	.11256	.33698	.59418	.86414
		5TH	197.52780	.08769	.26253	.46290	.67321 .89079
.40	.30	1ST	7.60249	.55623			
		2ND	29.60600	.24799	.73387		
		3RD	65.88782	.15491	.45839	.81656	
		4TH	116.43204	.11082	.32793	.58416	.86000
		5TH	181.23810	.08542	.25278	.45028	.66290 .88685
.40	.40	1ST	7.72161	.56480			
		2ND	28.23606	.24957	.73263		
		3RD	61.39641	.15359	.45083	.81243	
		4TH	107.19079	.10842	.31824	.57348	.85555
		5TH	165.61856	.08260	.24247	.43694	.65185 .88261
.40	.50	1ST	7.81954	.57244			
		2ND	26.86962	.25016	.73103		
		3RD	57.03213	.15147	.44258	.80801	
		4TH	98.29884	.10537	.30788	.56207	.85078
		5TH	150.66916	.07926	.23159	.42280	.63997 .87801
.40	.60	1ST	7.89520	.57922			
		2ND	25.50630	.24975	.72905		
		3RD	52.79481	.14854	.43356	.80327	
		4TH	89.75611	.10168	.29677	.54983	.84562
		5TH	136.38979	.07541	.22010	.40778	.62715 .87301
.40	.80	1ST	7.97481	.59040			
		2ND	22.78702	.24577	.72381		
		3RD	44.69982	.14018	.41281	.79260	
		4TH	73.71740	.09239	.27208	.52239	.83394
		5TH	109.84064	.06627	.19515	.37468	.59814 .86153
.40	1.00	1ST	7.94921	.59862			
		2ND	20.07249	.23707	.71653		
		3RD	37.10783	.12824	.38759	.77990	
		4TH	59.07225	.08056	.24347	.48992	.81990
		5TH	85.96933	.05535	.16730	.33664	.56338 .84752

TABLE 3. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF SYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.50	.10	1ST	7.70451	.55026			
		2ND	33.22605	.25206	.74052		
		3RD	76.58974	.16241	.47714	.82630	
		4TH	137.76862	.11924	.35031	.60664	.86926
		5TH	216.76231	.09393	.27596	.47790	.68478 .89523
.50	.20	1ST	7.85944	.56006			
		2ND	31.81981	.25513	.73985		
		3RD	71.79048	.16235	.47078	.82272	
		4TH	127.75066	.11787	.34179	.59730	.86545
		5TH	199.69988	.09196	.26667	.46602	.57523 .89163
.50	.30	1ST	7.99483	.56885			
		2ND	30.41752	.25725	.73888		
		3RD	67.11858	.16150	.46383	.81892	
		4TH	118.08217	.11584	.33269	.58737	.86137
		5TH	183.30764	.08943	.25686	.45348	.66502 .88775
.50	.40	1ST	8.10973	.57673			
		2ND	29.01891	.25842	.73758		
		3RD	62.57391	.15987	.45625	.81486	
		4TH	108.76303	.11316	.32296	.57679	.85700
		5TH	167.58556	.08637	.24649	.44022	.65408 .88357
.50	.50	1ST	8.20310	.58375			
		2ND	27.62368	.25864	.73594		
		3RD	58.15633	.15746	.44798	.81053	
		4TH	99.79315	.10986	.31255	.56549	.85231
		5TH	152.53357	.08279	.23555	.42617	.64232 .87904
.50	.60	1ST	8.27384	.59000			
		2ND	26.23144	.25790	.73394		
		3RD	53.86561	.15426	.43894	.80588	
		4TH	91.17242	.10592	.30141	.55336	.84724
		5TH	138.15160	.07872	.22399	.41123	.62962 .87411
.50	.80	1ST	8.34252	.60029			
		2ND	23.45375	.25331	.72869		
		3RD	45.66350	.14539	.41819	.79542	
		4TH	74.97754	.09617	.27664	.52616	.83577
		5TH	111.39706	.06915	.19890	.37830	.60090 .86282
.50	1.00	1ST	8.30437	.60783			
		2ND	20.67981	.24409	.72147		
		3RD	37.95372	.13296	.39300	.78298	
		4TH	60.17573	.08388	.24794	.49397	.82200
		5TH	87.32002	.05781	.17086	.34041	.56647 .84904

TABLE 3. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF SYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)				
.60	.10	1ST	8.11171	.56362				
		2ND	34.10197	.26187	.74545			
		3RD	77.93421	.16950	.48250	.82845		
		4TH	139.58179	.12473	.35504	.60961	.87048	
		5TH	219.04425	.09839	.28008	.48089	.68668	.89601
.60	.20	1ST	8.26298	.57262				
		2ND	32.66723	.26448	.74471			
		3RD	73.08178	.16909	.47609	.82494		
		4TH	129.48601	.12306	.34648	.60035	.86672	
		5TH	201.87928	.09615	.27073	.46909	.67722	.89246
.60	.30	1ST	8.39438	.58070				
		2ND	31.23633	.26619	.74367			
		3RD	68.35665	.16793	.46911	.82121		
		4TH	119.73962	.12076	.33734	.59052	.86271	
		5TH	185.38451	.09338	.26086	.45663	.66711	.88863
.60	.40	1ST	8.50494	.58795				
		2ND	29.80902	.26698	.74232			
		3RD	63.75872	.16600	.46151	.81723		
		4TH	110.34258	.11783	.32757	.58004	.85842	
		5TH	169.55988	.09008	.25044	.44345	.65627	.88451
.60	.50	1ST	8.59363	.59443				
		2ND	28.38496	.26686	.74065			
		3RD	59.28779	.16332	.45323	.81298		
		4TH	101.29476	.11428	.31713	.56883	.85381	
		5TH	154.40532	.08628	.23943	.42947	.64462	.88005
.60	.60	1ST	8.65935	.60019				
		2ND	26.96374	.26580	.73862			
		3RD	54.94365	.15986	.44419	.80841		
		4TH	92.59603	.11011	.30595	.55681	.84883	
		5TH	139.92068	.08199	.22782	.41462	.63205	.87520
.60	.80	1ST	8.71689	.60968				
		2ND	24.12752	.26065	.73338			
		3RD	46.63435	.15051	.42345	.79816		
		4TH	76.24491	.09992	.28111	.52986	.83756	
		5TH	112.96074	.07201	.20259	.38185	.60360	.86409
.60	1.00	1ST	8.66598	.61661				
		2ND	21.29402	.25094	.72623			
		3RD	38.82667	.13762	.39829	.78597		
		4TH	61.28636	.08719	.25233	.49794	.82405	
		5TH	88.67790	.06026	.17439	.34413	.56951	.85054

TABLE 3. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF SYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)			
.80	.10	1ST	8.94826	.58784			
		2ND	35.87586	.28040	.75467		
		3RD	80.64518	.18308	.49272	.83258	
		4TH	143.23018	.13531	.36417	.61535	.87283
		5TH	223.63016	.10703	.28805	.48672	.69038 .89753
.80	.20	1ST	9.09185	.59547			
		2ND	34.38400	.28220	.75380		
		3RD	75.68635	.18205	.48625	.82919	
		4TH	132.97867	.13311	.35553	.60627	.86919
		5TH	206.26014	.10431	.27860	.47507	.68109 .89407
.80	.30	1ST	9.21490	.60236			
		2ND	32.89580	.28317	.75266		
		3RD	70.85474	.18032	.47923	.82559	
		4TH	123.07650	.13031	.34632	.59661	.86531
		5TH	189.56025	.10107	.26863	.46276	.67117 .89035
.80	.40	1ST	9.31647	.60854			
		2ND	31.41095	.28330	.75124		
		3RD	66.15020	.17786	.47160	.82176	
		4TH	113.52360	.12691	.33650	.58632	.86116
		5TH	173.53047	.09734	.25811	.44973	.66054 .88634
.80	.50	1ST	9.39549	.61408			
		2ND	29.92909	.28256	.74951		
		3RD	61.57252	.17469	.46331	.81766	
		4TH	104.31985	.12291	.32600	.57532	.85670
		5TH	158.17068	.09313	.24701	.43591	.64911 .88201
.80	.60	1ST	9.45086	.61901			
		2ND	28.44975	.28093	.74746		
		3RD	57.12144	.17076	.45427	.81326	
		4TH	95.46505	.11832	.31477	.56351	.85189
		5TH	143.48078	.08844	.23529	.42122	.63678 .87730
.80	.80	1ST	9.48552	.62712			
		2ND	25.49611	.27478	.74223		
		3RD	48.59751	.16052	.43357	.80340	
		4TH	78.80130	.10730	.28982	.53702	.84102
		5TH	116.10986	.07768	.20982	.38878	.60887 .86654
.80	1.00	1ST	9.40851	.63297			
		2ND	22.54303	.26417	.73523		
		3RD	40.57372	.14678	.40850	.79168	
		4TH	63.52904	.09374	.26089	.50562	.82800
		5TH	91.41526	.06515	.18131	.35138	.57542 .85343

TABLE 3. NATURAL FREQUENCIES AND NODES FOR TAPERED FREE-FREE BEAMS OF SYMMETRICAL MODE

Ψ	Φ	MODE	FREQUENCY CONSTANT, K	LOCATIONS OF NODES (X/L)				
1.00	.10	1ST	9.81405	.60923				
		2ND	37.67907	.29763	.76314			
		3RD	83.38550	.19593	.50235	.83648		
		4TH	146.90791	.14543	.37287	.62086	.87509	
		5TH	228.24542	.11533	.29569	.49236	.69396	.89900
1.00	.20	1ST	9.94950	.61577				
		2ND	36.12995	.29874	.76217			
		3RD	78.32020	.19437	.49584	.83321		
		4TH	136.50064	.14276	.36418	.61194	.87156	
		5TH	210.67030	.11217	.28616	.48084	.68484	.89563
1.00	.30	1ST	10.06378	.62168				
		2ND	34.58428	.29908	.76095			
		3RD	73.38202	.19214	.48880	.82974		
		4TH	126.44264	.13951	.35492	.60246	.86781	
		5TH	193.76527	.10853	.27611	.46868	.67510	.89201
1.00	.40	1ST	10.15593	.62700				
		2ND	33.04173	.29863	.75947			
		3RD	68.57077	.18922	.48116	.82604		
		4TH	116.73384	.13569	.34505	.59235	.86379	
		5TH	177.53030	.10441	.26551	.45580	.66467	.88811
1.00	.50	1ST	10.22488	.63177				
		2ND	31.50187	.29736	.75771			
		3RD	63.88623	.18560	.47287	.82209		
		4TH	107.37406	.13129	.33451	.58154	.85947	
		5TH	161.96526	.09982	.25433	.44214	.65345	.88390
1.00	.60	1ST	10.26950	.63601				
		2ND	29.95420	.29524	.75564			
		3RD	59.32808	.18125	.46384	.81785		
		4TH	98.35312	.12631	.32325	.56993	.85482	
		5TH	147.07000	.09477	.24252	.42761	.64134	.87933
1.00	.80	1ST	10.28050	.64296				
		2ND	26.89264	.28820	.75047			
		3RD	50.58920	.17022	.44321	.80834		
		4TH	81.38650	.11453	.29822	.54389	.84432	
		5TH	119.28795	.08328	.21685	.39549	.61395	.86889
1.00	1.00	1ST	10.17662	.64792				
		2ND	23.81939	.27682	.74362			
		3RD	42.34886	.15570	.41825	.79707		
		4TH	65.80021	.10021	.26919	.51299	.83176	
		5TH	94.18135	.07001	.18807	.35841	.58111	.85621

TABLE 4. NATURAL FREQUENCIES FOR TRUNCATED BEAMS

		C = 0.2		C = 0.4	
Ψ	Φ	1ST MODE	2ND MODE	1ST MODE	2ND MODE
.1	.0	3.67847	22.36876	3.61365	22.22533
.2	.0	3.84786	22.70905	3.71272	22.41816
.3	.0	4.02157	23.05519	3.81430	22.61243
.4	.0	4.20091	23.40771	3.91801	22.80770
.5	.0	4.38517	23.76588	4.02307	23.00573
.6	.0	4.57712	24.13146	4.13134	23.20523
.7	.0	4.77262	24.50256	4.24163	23.40584
.8	.0	4.97587	24.88047	4.35377	23.60921
.9	.0	5.18301	25.26468	4.46853	23.81437
1.0	.0	5.39691	25.65562	4.58573	24.02130
.0	.1	3.61104	21.40556	3.56582	21.56926
.0	.2	3.70551	20.77436	3.61455	21.10498
.0	.3	3.79561	20.14155	3.66175	20.64266
.0	.4	3.88164	19.50751	3.70660	20.18308
.0	.5	3.96387	18.87350	3.75005	19.72495
.0	.6	4.04053	18.24194	3.79130	19.27075
.0	.7	4.11409	17.61204	3.83125	18.82074
.0	.8	4.18075	16.98365	3.86828	18.36944
.0	.9	4.23912	16.36086	3.90247	17.97842
.0	1.0	4.29265	15.74243	3.93432	17.59643
.1	.1	3.77736	21.73113	3.66352	21.75592
.2	.2	4.04253	21.41178	3.81260	21.47170
.3	.3	4.31454	21.07969	3.96323	21.18252
.4	.4	4.58885	20.73267	4.11464	20.88849
.5	.5	4.86505	20.37156	4.26638	20.59206
.6	.6	5.14136	19.99895	4.41749	20.29139
.7	.7	5.41396	19.61430	4.56803	19.98790
.8	.8	5.68160	19.21557	4.71720	19.68703
.9	.9	5.94408	18.80675	4.86446	19.40364
1.0	1.0	6.19721	18.38376	5.00722	19.13450

TABLE 5. APPROXIMATE FUNDAMENTAL FREQUENCIES

Ψ	Φ	C	UPPER BOUND	LOWER BOUND	Ψ	Φ	C	UPPER BOUND	LOWER BOUND
.00	.00	.00	3.46410	3.53009	.00	.60	.00	4.57891	5.13806
		.10	3.46410	3.53009			.10	4.13003	4.58113
		.20	3.46410	3.53009			.20	3.92379	4.27828
		.30	3.46410	3.53009			.30	3.79515	4.07590
		.40	3.46410	3.53009			.40	3.70554	3.92952
		.50	3.46410	3.53009			.50	3.63910	3.81882
		.75	3.46410	3.53009			.75	3.52972	3.63569
.00	.10	.00	3.68862	3.79204	.00	.80	.00	4.79400	5.69898
		.10	3.59159	3.68841			.10	4.27443	4.98299
		.20	3.55178	3.64280			.20	4.02933	4.56564
		.30	3.52681	3.61297			.30	3.87526	4.28366
		.40	3.50935	3.59139			.40	3.76697	4.07954
		.50	3.49645	3.57492			.50	3.68584	3.92557
		.75	3.47570	3.54703			.75	3.54938	3.67299
.00	.20	.00	3.89954	4.05588	.00	1.00	.00	4.89898	6.27495
		.10	3.71413	3.85364			.10	4.36092	5.40881
		.20	3.63587	3.76033			.20	4.10184	4.87170
		.30	3.58693	3.69910			.30	3.93573	4.50434
		.40	3.55281	3.65480			.40	3.81669	4.23801
		.50	3.52763	3.62107			.50	3.72577	4.03760
		.75	3.48703	3.56424			.75	3.56785	3.71133
.00	.30	.00	4.09560	4.32206	.10	.00	.00	3.78444	3.86568
		.10	3.83053	4.02565			.10	3.67314	3.75169
		.20	3.71576	3.88267			.20	3.62115	3.69739
		.30	3.64415	3.78846			.30	3.58526	3.65957
		.40	3.59431	3.72032			.40	3.55780	3.63046
		.50	3.55755	3.66854			.50	3.53561	3.60684
		.75	3.49811	3.58171			.75	3.49402	3.56231
.00	.40	.00	4.27532	4.59096	.10	.10	.00	4.00639	4.13031
		.10	3.93954	4.20432			.10	3.80288	3.91666
		.20	3.79081	4.00978			.20	3.71002	3.81446
		.30	3.69814	3.88105			.30	3.64854	3.74524
		.40	3.63371	3.78795			.40	3.60329	3.69349
		.50	3.58616	3.71732			.50	3.56805	3.65270
		.75	3.50892	3.59944			.75	3.50561	3.57944
.00	.50	.00	4.43706	4.86287	.10	.20	.00	4.21433	4.39723
		.10	4.03983	4.38953			.10	3.92704	4.08853
		.20	3.86039	4.14166			.20	3.79498	3.93642
		.30	3.74859	3.97686			.30	3.70906	3.83419
		.40	3.67084	3.85768			.40	3.64691	3.75866
		.50	3.61336	3.76741			.50	3.59927	3.69991
		.75	3.51946	3.61744			.75	3.51693	3.59684

TABLE 5. APPROXIMATE FUNDAMENTAL FREQUENCIES

Ψ	Φ	C	UPPER BOUND	LOWER BOUND	Ψ	Φ	C	UPPER BOUND	LOWER BOUND
.10	.30	.00	4.40690	4.66685	.20	.00	.00	4.11047	4.20899
		.10	4.04439	4.26717			.10	3.88993	3.98278
		.20	3.87539	4.06324			.20	3.78311	3.87085
		.30	3.76650	3.92643			.30	3.70949	3.79299
		.40	3.68849	3.82597			.40	3.65338	3.73330
		.50	3.62920	3.74844			.50	3.60824	3.68508
		.75	3.52800	3.61450			.75	3.52414	3.59481
.10	.40	.00	4.58258	4.93946	.20	.10	.00	4.32982	4.47647
		.10	4.15365	4.45242			.10	4.02164	4.15437
		.20	3.95063	4.19490			.20	3.87305	3.99235
		.30	3.82055	4.02195			.30	3.77328	3.88149
		.40	3.72787	3.89542			.40	3.69909	3.79810
		.50	3.65777	3.79830			.50	3.64075	3.73200
		.75	3.53879	3.63242			.75	3.53571	3.61213
.10	.50	.00	4.73962	5.21532	.20	.20	.00	4.53467	4.74663
		.10	4.25347	4.64414			.10	4.14712	4.33284
		.20	4.02000	4.33135			.20	3.95874	4.11879
		.30	3.87085	4.12073			.30	3.83414	3.97333
		.40	3.76488	3.96700			.40	3.74284	3.86506
		.50	3.68489	3.84949			.50	3.67201	3.78026
		.75	3.54930	3.65061			.75	3.54703	3.62971
.10	.60	.00	4.87608	5.49465	.20	.30	.00	4.72361	5.01978
		.10	4.34245	4.84219			.10	4.26510	4.51802
		.20	4.08282	4.47258			.20	4.03955	4.25014
		.30	3.91706	4.22278			.30	3.89174	4.06849
		.40	3.79936	4.04072			.40	3.78446	3.93419
		.50	3.71049	3.90201			.50	3.70193	3.82988
		.75	3.55954	3.66906			.75	3.55808	3.64757
.10	.80	.00	5.07807	6.06430	.20	.40	.00	4.89506	5.29619
		.10	4.48208	5.25671			.10	4.37428	4.70976
		.20	4.18599	4.76927			.20	4.11480	4.38636
		.30	3.99587	4.43667			.30	3.94575	4.16697
		.40	3.86007	4.19457			.40	3.82378	4.00548
		.50	3.75683	4.01104			.50	3.73043	3.88084
		.75	3.57913	3.70675			.75	3.56885	3.66568
.10	1.00	.00	5.16633	6.64945	.20	.50	.00	5.04723	5.57605
		.10	4.56063	5.69483			.10	4.47328	4.90791
		.20	4.25446	5.08473			.20	4.18382	4.52742
		.30	4.05419	4.66363			.30	3.99583	4.26876
		.40	3.90864	4.35697			.40	3.86064	4.07894
		.50	3.79617	4.12539			.50	3.75745	3.93314
		.75	3.59752	3.74550			.75	3.57934	3.68407

TABLE 5. APPROXIMATE FUNDAMENTAL FREQUENCIES

Ψ	Φ	C	UPPER BOUND	LOWER BOUND	Ψ	Φ	C	UPPER BOUND	LOWER BOUND
.20	.60	.00	5.17811	5.85955	.30	.30	.00	5.04571	5.38093
		.10	4.56070	5.11232			.10	4.49254	4.77819
		.20	4.24589	4.67330			.20	4.20822	4.44343
		.30	4.04162	4.37386			.30	4.01987	4.21469
		.40	3.89487	4.15456			.40	3.88223	4.04501
		.50	3.78290	3.98679			.50	3.77573	3.91288
		.75	3.58955	3.70272			.75	3.58835	3.68092
.20	.80	.00	5.36656	6.43796	.30	.40	.00	5.21275	5.66119
		.10	4.69487	5.53927			.10	4.60130	4.97633
		.20	4.34633	4.97934			.20	4.28334	4.58425
		.30	4.11895	4.59396			.30	4.07378	4.31618
		.40	3.95475	4.31229			.40	3.92146	4.11817
		.50	3.82880	4.09811			.50	3.80416	3.96495
		.75	3.60907	3.74081			.75	3.59910	3.69923
.20	1.00	.00	5.43765	7.03230	.30	.50	.00	5.35985	5.94509
		.10	4.76478	5.98943			.10	4.69915	5.18080
		.20	4.41039	5.30421			.20	4.35183	4.72995
		.30	4.17494	4.82725			.30	4.12355	4.42101
		.40	4.00209	4.47868			.40	3.95812	4.19353
		.50	3.86750	4.21482			.50	3.83106	4.01838
		.75	3.62738	3.77995			.75	3.60957	3.71781
.30	.00	.00	4.44230	4.56015	.30	.60	.00	5.48494	6.23279
		.10	4.11441	4.22339			.10	4.78465	5.39144
		.20	3.95000	4.05059			.20	4.41298	4.88048
		.30	3.83681	3.93044			.30	4.16883	4.52919
		.40	3.75086	3.83867			.40	3.99206	4.27108
		.50	3.68199	3.76484			.50	3.85634	4.07317
		.75	3.55446	3.62758			.75	3.61975	3.73666
.30	.10	.00	4.65893	4.83064	.30	.80	.00	5.65943	6.81998
		.10	4.24779	4.40155			.10	4.91267	5.83058
		.20	4.04088	4.17655			.20	4.51033	5.19589
		.30	3.90105	4.02181			.30	4.24449	4.75556
		.40	3.79676	3.90525			.40	4.05104	4.43274
		.50	3.71456	3.81282			.50	3.90175	4.18682
		.75	3.56602	3.64509			.75	3.63921	3.77515
.30	.20	.00	4.86056	5.10415	.30	1.00	.00	5.71288	7.42349
		.10	4.37426	4.58654			.10	4.97328	6.29253
		.20	4.12718	4.30751			.20	4.56961	5.53018
		.30	3.96218	4.11657			.30	4.29796	4.99526
		.40	3.84061	3.97403			.40	4.09704	4.60316
		.50	3.74583	3.86217			.50	3.93977	4.30591
		.75	3.57732	3.66287			.75	3.65743	3.81470

TABLE 5. APPROXIMATE FUNDAMENTAL FREQUENCIES

Ψ	Φ	C	UPPER BOUND	LOWER BOUND	Ψ	Φ	C	UPPER BOUND	LOWER BOUND
.40	.00	.00	4.77996	4.91929	.40	.60	.00	5.79655	6.61438
		.10	4.34650	4.47354			.10	5.01420	5.67949
		.20	4.12184	4.23667			.20	4.58408	5.09417
		.30	3.96724	4.07198			.30	4.29869	4.68884
		.40	3.85026	3.94659			.40	4.09093	4.39031
		.50	3.75687	3.84613			.50	3.93080	4.16117
		.75	3.58497	3.66064			.75	3.65014	3.77089
.40	.10	.00	4.99375	5.19293	.40	.80	.00	5.95664	7.21036
		.10	4.48122	4.65818			.10	5.13539	6.13056
		.20	4.21353	4.36715			.20	4.67798	5.41897
		.30	4.03187	4.16627			.30	4.37251	4.92155
		.40	3.89632	4.01499			.40	4.14892	4.55595
		.50	3.78949	3.89519			.50	3.97569	4.27718
		.75	3.59653	3.67834			.75	3.66953	3.80978
.40	.20	.00	5.19199	5.46988	.40	1.00	.00	5.99199	7.82303
		.10	4.60836	4.84961			.10	5.18602	6.60404
		.20	4.30027	4.50267			.20	4.73208	5.76267
		.30	4.09320	4.26398			.30	4.42325	5.16770
		.40	3.94022	4.08561			.40	4.19350	4.73045
		.50	3.82076	3.94564			.50	4.01298	4.39868
		.75	3.60782	3.69631			.75	3.68766	3.84975
.40	.30	.00	5.37318	5.75035	.50	.00	.00	5.12348	5.28650
		.10	4.72660	5.04762			.10	4.58609	4.73319
		.20	4.38141	4.64317			.20	4.29863	4.42920
		.30	4.15091	4.36511			.30	4.10081	4.21766
		.40	3.98181	4.15846			.40	3.95158	4.05711
		.50	3.85061	3.99746			.50	3.83290	3.92898
		.75	3.61883	3.71456			.75	3.61569	3.69398
.40	.40	.00	5.53563	6.03450	.50	.10	.00	5.33427	5.56339
		.10	4.83460	5.25206			.10	4.72183	4.92424
		.20	4.45623	4.78862			.20	4.39098	4.56422
		.30	4.20463	4.46963			.30	4.16575	4.31491
		.40	4.02090	4.23353			.40	3.99776	4.12735
		.50	3.87895	4.05066			.50	3.86554	3.97914
		.75	3.62955	3.73307			.75	3.62724	3.71187
.40	.50	.00	5.67746	6.32247	.50	.20	.00	5.52896	5.84385
		.10	4.93095	5.46274			.10	4.84930	5.12200
		.20	4.52403	4.93897			.20	4.47803	4.70432
		.30	4.25400	4.57755			.30	4.22722	4.41562
		.40	4.05734	4.31081			.40	4.04169	4.19985
		.50	3.90571	4.10523			.50	3.89680	4.03069
		.75	3.63999	3.75184			.75	3.63851	3.73004

TABLE 5. APPROXIMATE FUNDAMENTAL FREQUENCIES

Ψ	Φ	C	UPPER BOUND	LOWER BOUND	Ψ	Φ	C	UPPER BOUND	LOWER BOUND
.50	.30	.00	5.70600	6.12806	.60	.00	.00	5.47284	5.66186
		.10	4.96716	5.32627			.10	4.83306	5.00233
		.20	4.55910	4.84944			.20	4.48037	4.62823
		.30	4.28485	4.51979			.30	4.23752	4.36756
		.40	4.08321	4.27460			.40	4.05484	4.17027
		.50	3.92658	4.08364			.50	3.91006	4.01341
		.75	3.64950	3.74848			.75	3.64662	3.72760
.50	.40	.00	5.86365	6.41614	.60	.10	.00	5.68047	5.94208
		.10	5.07406	5.53688			.10	4.96949	5.19968
		.20	4.63346	4.99953			.20	4.57324	4.76782
		.30	4.33830	4.62739			.30	4.30271	4.46781
		.40	4.12213	4.35159			.40	4.10111	4.24238
		.50	3.95481	4.13798			.50	3.94272	4.06468
		.75	3.66020	3.76719			.75	3.65815	3.74569
.50	.50	.00	6.00000	6.70820	.60	.20	.00	5.87142	6.22612
		.10	5.16857	5.75364			.10	5.09695	5.40365
		.20	4.70039	5.15454			.20	4.66044	4.91253
		.30	4.38721	4.73842			.30	4.36423	4.57156
		.40	4.15829	4.43082			.40	4.14503	4.31677
		.50	3.98141	4.19370			.50	3.97394	4.11736
		.75	3.67061	3.78617			.75	3.66940	3.76406
.50	.60	.00	6.11289	7.00434	.60	.30	.00	6.04411	6.51410
		.10	5.24922	5.97637			.10	5.21410	5.61406
		.20	4.75916	5.31443			.20	4.74127	5.06228
		.30	4.43120	4.85286			.30	4.42172	4.67879
		.40	4.19150	4.51230			.40	4.18644	4.39344
		.50	4.00629	4.25082			.50	4.00364	4.17144
		.75	3.68073	3.80541			.75	3.68036	3.78269
.50	.80	.00	6.25815	7.60910	.60	.40	.00	6.19677	6.80614
		.10	5.36292	5.43911			.10	5.31955	5.83071
		.20	4.84923	5.64861			.20	4.81500	5.21703
		.30	4.50299	5.09196			.30	4.47482	4.78951
		.40	4.24840	4.68197			.40	4.22515	4.47239
		.50	4.05061	4.36921			.50	4.03174	4.22694
		.75	3.70004	3.84471			.75	3.69104	3.80160
.50	1.00	.00	6.27495	8.23093	.60	.50	.00	6.32744	7.10230
		.10	5.40292	6.92384			.10	5.41188	6.05342
		.20	4.89778	6.00168			.20	4.88089	5.37671
		.30	4.55081	5.34461			.30	4.52316	4.90368
		.40	4.29146	4.86060			.40	4.26098	4.55360
		.50	4.08714	4.49316			.50	4.05816	4.28383
		.75	3.71808	3.88509			.75	3.70143	3.82078

TABLE 5. APPROXIMATE FUNDAMENTAL FREQUENCIES

Ψ	Φ	C	UPPER BOUND	LOWER BOUND	Ψ	Φ	C	UPPER BOUND	LOWER BOUND
.60	.60	.00	6.43391	7.40267	.80	.30	.00	6.73607	7.31124
		.10	5.48960	6.28200			.10	5.72654	6.21672
		.20	4.93820	5.54127			.20	5.11899	5.50787
		.30	4.56637	5.02130			.30	4.70423	5.01000
		.40	4.29377	4.63708			.40	4.39840	4.63944
		.50	4.08282	4.34213			.50	4.16107	4.35199
		.75	3.71151	3.84023			.75	3.74270	3.85200
.60	.80	.00	6.56390	8.01622	.80	.40	.00	6.87814	7.61123
		.10	5.59514	6.75613			.10	5.82809	6.44505
		.20	5.02406	5.88482			.20	5.19093	5.67193
		.30	4.63594	5.26684			.30	4.75636	5.12703
		.40	4.34950	4.81082			.40	4.43656	4.72235
		.50	4.12653	4.46294			.50	4.18885	4.40984
		.75	3.73074	3.87994			.75	3.75332	3.87131
.60	1.00	.00	6.56171	8.64718	.80	.50	.00	6.99682	7.91563
		.10	5.62389	7.25185			.10	5.91505	6.67923
		.20	5.06668	6.24724			.20	5.25420	5.84094
		.30	4.68063	5.52604			.30	4.80330	5.24757
		.40	4.39093	4.99362			.40	4.47163	4.80759
		.50	4.16224	4.58935			.50	4.21485	4.46912
		.75	3.74869	3.92073			.75	3.76364	3.89089
.80	.00	.00	6.18902	6.43723	.80	.60	.00	7.08982	8.22447
		.10	5.34864	5.56883			.10	5.98592	6.91909
		.20	4.85869	5.04607			.20	5.30803	6.01484
		.30	4.52044	4.68026			.30	4.84467	5.37163
		.40	4.26723	4.40465			.40	4.50342	4.89514
		.50	4.06786	4.18708			.50	4.23899	4.52983
		.75	3.70907	3.79571			.75	3.77365	3.91075
.80	.10	.00	6.38977	6.72429	.80	.80	.00	7.18799	8.85557
		.10	5.48542	5.77840			.10	6.07323	7.41518
		.20	4.95214	5.19487			.20	5.38434	6.37703
		.30	4.58590	4.78660			.30	4.90919	5.63019
		.40	4.31356	4.48058			.40	4.55650	5.07717
		.50	4.10049	4.24061			.50	4.28135	4.65554
		.75	3.72057	3.81420			.75	3.79271	3.95129
.80	.20	.00	6.57267	7.01561	.80	1.00	.00	7.14647	9.50473
		.10	5.61184	5.99444			.10	6.07763	7.93210
		.20	5.03915	5.34883			.20	5.41391	6.75801
		.30	4.64728	4.89652			.30	4.94702	5.90259
		.40	4.35734	4.55884			.40	4.59437	5.26844
		.50	4.13159	4.29558			.50	4.31528	4.78698
		.75	3.73178	3.83296			.75	3.81046	3.99292

TABLE 5. APPROXIMATE FUNDAMENTAL FREQUENCIES

Ψ	Φ	C	UPPER BOUND	LOWER BOUND	Ψ	Φ	C	UPPER BOUND	LOWER BOUND
1.00	.00	.00	6.92820	7.24569	1.00	.60	.00	7.76392	9.07980
		.10	5.89209	6.17242			.10	6.50219	7.58991
		.20	5.25670	5.49065			.20	5.69329	6.51501
		.30	4.81608	5.01052			.30	5.13355	5.74018
		.40	4.48749	4.65004			.40	4.71991	5.16478
		.50	4.23031	4.36731			.50	4.39933	4.72442
		.75	3.77234	3.86499			.75	3.83656	3.98247
1.00	.10	.00	7.12130	7.53977	1.00	.80	.00	7.82856	9.72840
		.10	6.02787	6.39369			.10	6.56883	8.10688
		.20	5.35007	5.64868			.20	5.75852	6.89566
		.30	4.88149	5.12308			.30	5.19222	6.01191
		.40	4.53373	4.72988			.40	4.76994	5.35527
		.50	4.26284	4.42316			.50	4.44016	4.85515
		.75	3.78380	3.88388			.75	3.85545	4.02384
1.00	.20	.00	7.29537	7.83849	1.00	1.00	.00	7.74597	10.39568
		.10	6.15190	6.62122			.10	6.54654	8.64398
		.20	5.43621	5.81190			.20	5.77350	7.29493
		.30	4.94241	5.23930			.30	5.22233	6.29764
		.40	4.57721	4.81212			.40	4.80384	5.55516
		.50	4.29374	4.48049			.50	4.47214	4.99172
		.75	3.79496	3.90304			.75	3.87298	4.06632
1.00	.30	.00	7.44868	8.14184	.25	.25	.00	4.79257	5.06144
		.10	6.26280	6.85480			.10	4.31996	4.55190
		.20	5.51437	5.98022			.20	4.08352	4.27855
		.30	4.99846	5.35914			.30	3.92706	4.09233
		.40	4.61776	4.89673			.40	3.81259	3.95397
		.50	4.32292	4.53928			.50	3.72391	3.84593
		.75	3.80583	3.92248			.75	3.56771	3.65520
1.00	.40	.00	7.57934	8.44984	.75	.75	.00	7.01561	8.48425
		.10	6.35914	7.09423			.10	5.93616	7.12264
		.20	5.58379	6.15356			.20	5.27732	6.16033
		.30	5.04926	5.48258			.30	4.82584	5.47252
		.40	4.65518	4.98371			.40	4.49205	4.96365
		.50	4.35030	4.59953			.50	4.23235	4.57509
		.75	3.81638	3.94220			.75	3.77249	3.92315
1.00	.50	.00	7.68521	8.76249	.90	.90	.00	7.49528	9.61462
		.10	6.43944	7.33933			.10	6.32607	8.01807
		.20	5.64359	6.33185			.20	5.58736	6.82582
		.30	5.09442	5.60960			.30	5.07015	5.95653
		.40	4.68929	5.07306			.40	4.68243	5.31135
		.50	4.37580	4.66125			.50	4.37786	4.82073
		.75	3.82663	3.96220			.75	3.83297	4.00830

TABLE 6. RADII OF GYRATION FOR DIFFERENT CROSS-SECTIONS

γ	β	RADIUS/h	γ	β	RADIUS/h	γ	β	RADIUS/h
1.00	1.00	.40825	2.00	1.00	.47809	4.00	1.00	.52298
	1.25	.42008		1.25	.48467		1.25	.52641
	1.50	.43033		1.50	.49042		1.50	.52943
	1.75	.43930		1.75	.49549		1.75	.53212
	2.00	.44721		2.00	.50000		2.00	.53452
	2.50	.46057		2.50	.50767		2.50	.53864
	3.00	.47140		3.00	.51394		3.00	.54203
	3.50	.48038		3.50	.51918		3.50	.54488
	4.00	.48795		4.00	.52361		4.00	.54730
	5.00	.50000		5.00	.53071		5.00	.55120
	7.00	.51640		7.00	.54045		7.00	.55658
	10.00	.53108		10.00	.54924		10.00	.56148
1.25	1.00	.43355	2.50	1.00	.49507	5.00	1.00	.53300
	1.25	.44345		1.25	.50043		1.25	.53576
	1.50	.45204		1.50	.50513		1.50	.53821
	1.75	.45958		1.75	.50929		1.75	.54038
	2.00	.46625		2.00	.51299		2.00	.54233
	2.50	.47753		2.50	.51930		2.50	.54566
	3.00	.48671		3.00	.52448		3.00	.54842
	3.50	.49433		3.50	.52881		3.50	.55074
	4.00	.50076		4.00	.53248		4.00	.55271
	5.00	.51102		5.00	.53837		5.00	.55589
	7.00	.52502		7.00	.54647		7.00	.56030
	10.00	.53759		10.00	.55380		10.00	.56431
1.50	1.00	.45227	3.00	1.00	.50709	7.00	1.00	.54495
	1.25	.46075		1.25	.51161		1.25	.54694
	1.50	.46813		1.50	.51558		1.50	.54870
	1.75	.47463		1.75	.51909		1.75	.55027
	2.00	.48038		2.00	.52223		2.00	.55168
	2.50	.49014		2.50	.52759		2.50	.55410
	3.00	.49809		3.00	.53200		3.00	.55611
	3.50	.50471		3.50	.53569		3.50	.55779
	4.00	.51030		4.00	.53882		4.00	.55923
	5.00	.51924		5.00	.54385		5.00	.56156
	7.00	.53145		7.00	.55079		7.00	.56478
	10.00	.54244		10.00	.55708		10.00	.56773
1.75	1.00	.46667	3.50	1.00	.51605	10.00	1.00	.55427
	1.25	.47408		1.25	.51995		1.25	.55567
	1.50	.48055		1.50	.52338		1.50	.55691
	1.75	.48625		1.75	.52643		1.75	.55802
	2.00	.49130		2.00	.52915		2.00	.55902
	2.50	.49989		2.50	.53381		2.50	.56073
	3.00	.50691		3.00	.53764		3.00	.56216
	3.50	.51275		3.50	.54085		3.50	.56335
	4.00	.51770		4.00	.54358		4.00	.56438
	5.00	.52561		5.00	.54798		5.00	.56604
	7.00	.53645		7.00	.55404		7.00	.56834
	10.00	.54622		10.00	.55955		10.00	.57045



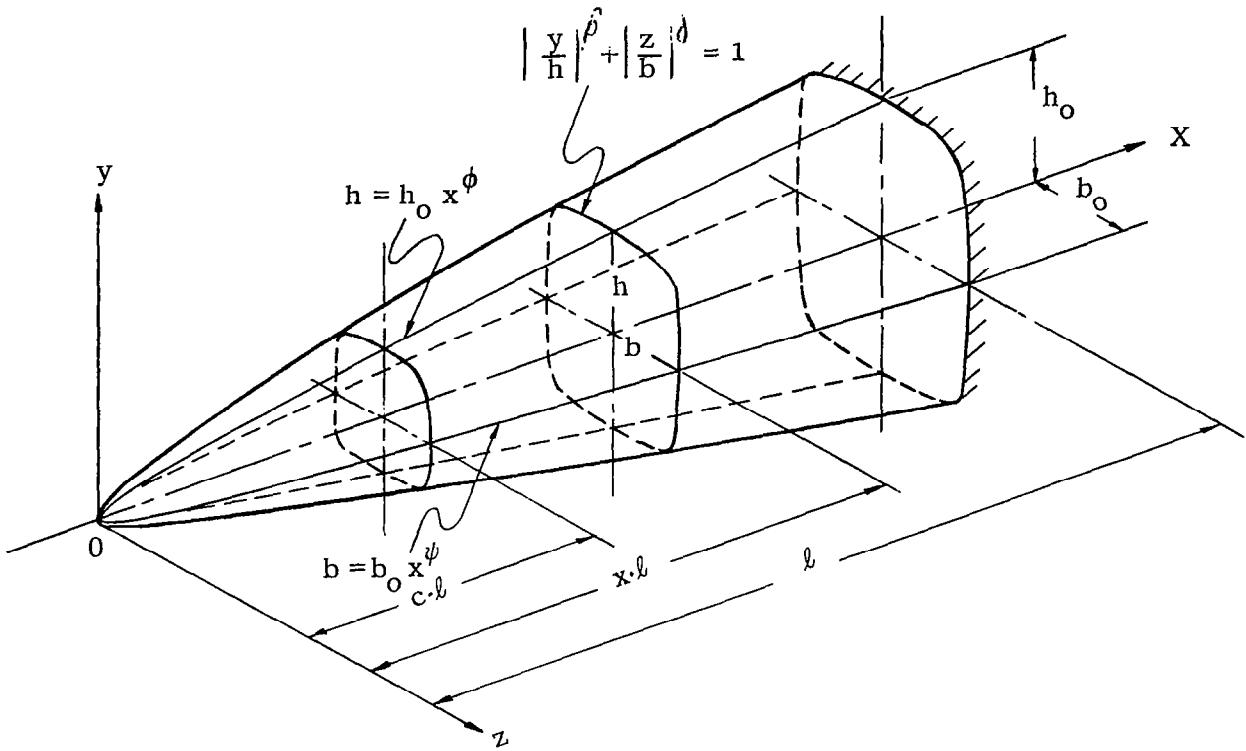


Fig. 1 Cantilever Beam

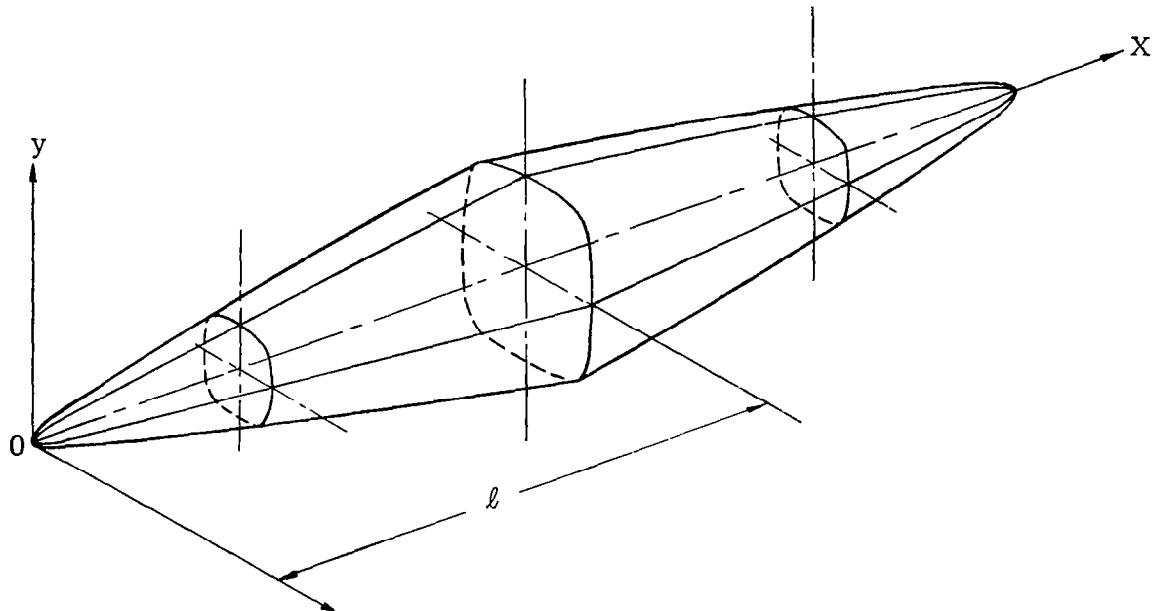


Fig. 2 Free-Free Beam

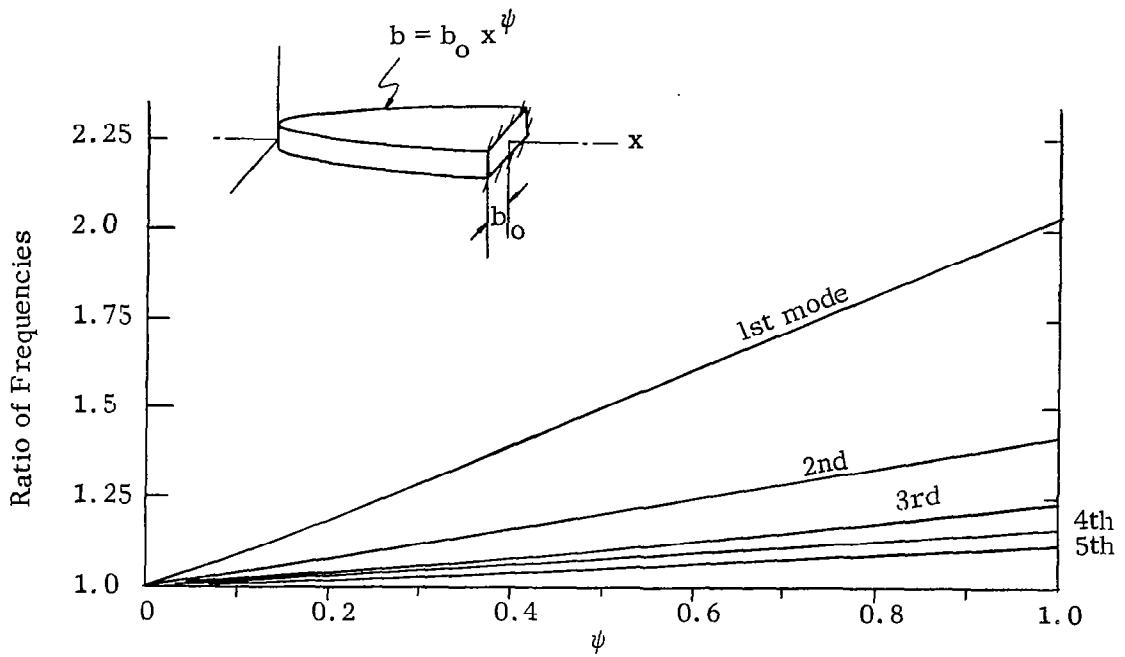


Fig. 3 Ratio of Frequencies of Cantilever Beams with Cross-Section Varying in Width to Those of Uniform Cross-Section

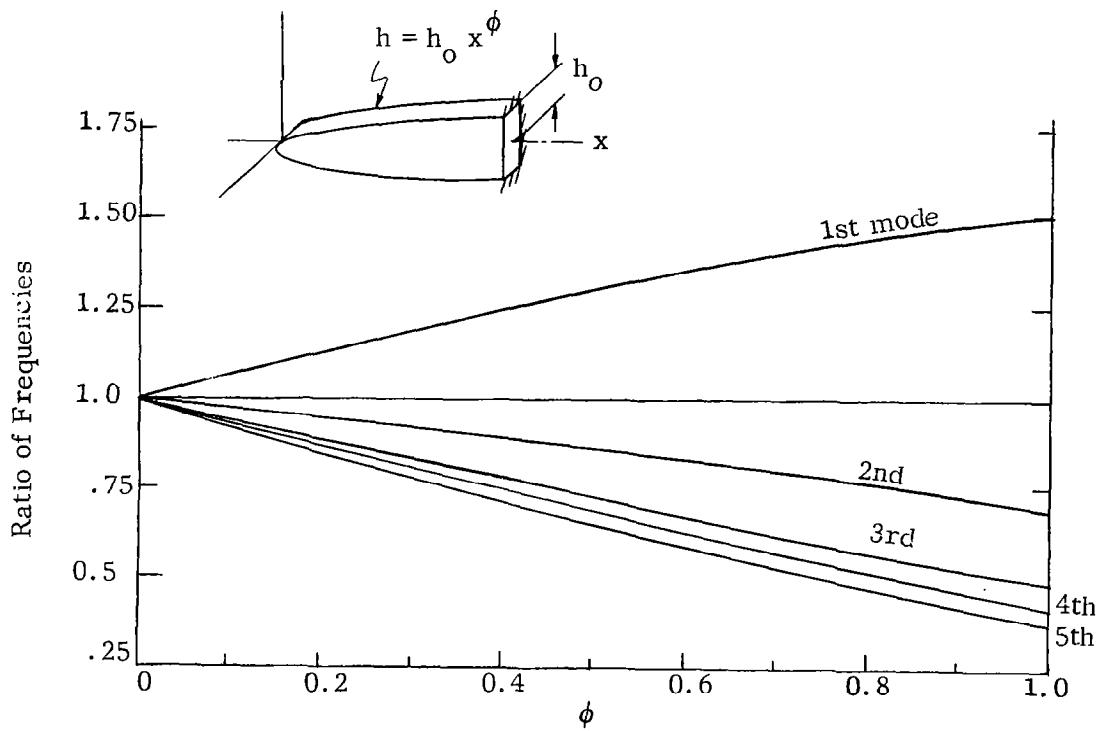


Fig. 4 Ratio of Frequencies of Cantilever Beams with Cross-Section Varying in Thickness to Those of Uniform Cross-Section

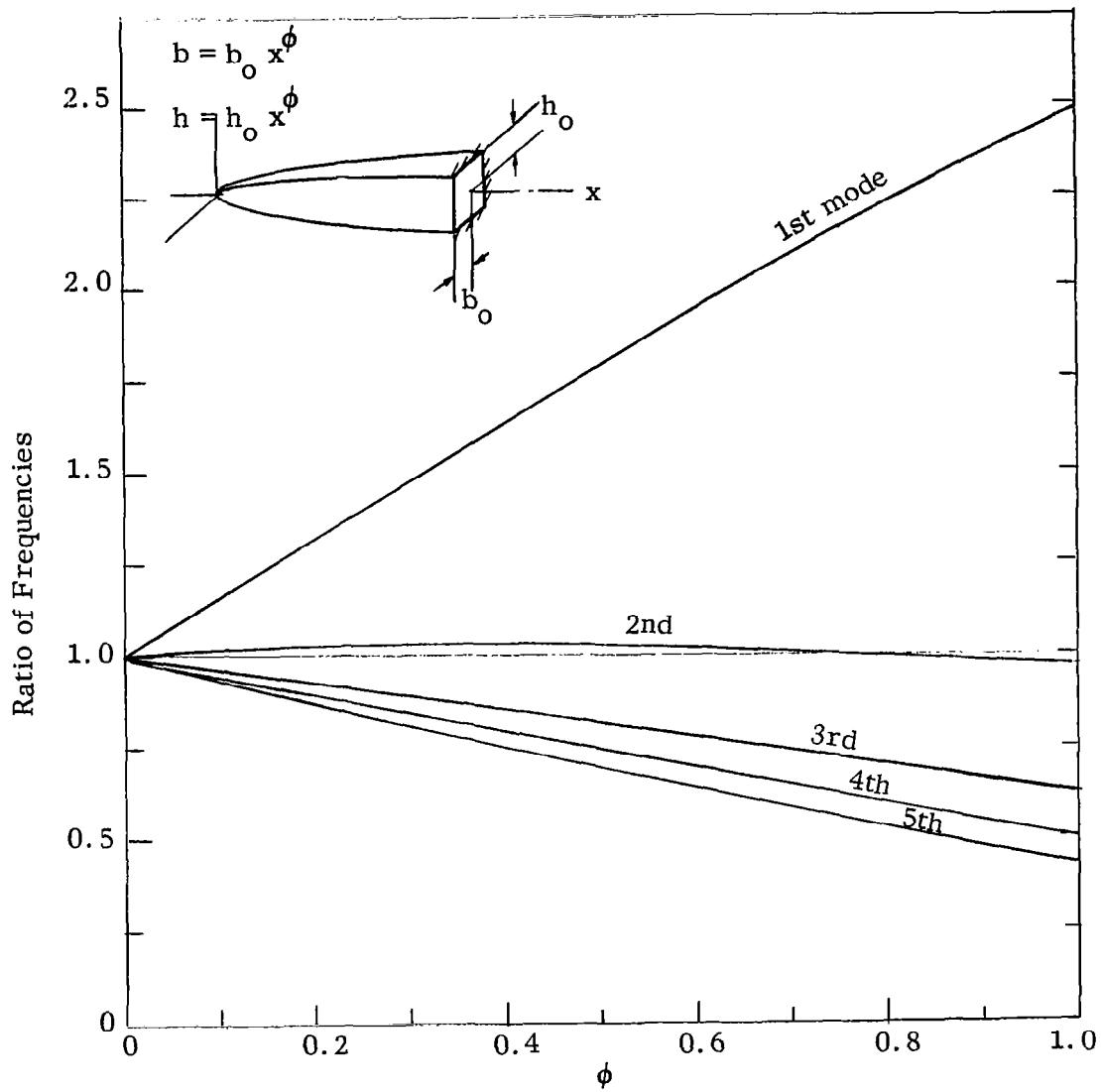


Fig. 5 Ratio of Frequencies of Cantilever Beams with Cross-Section Varying Both in Width and Thickness to Those of Uniform Cross-Section

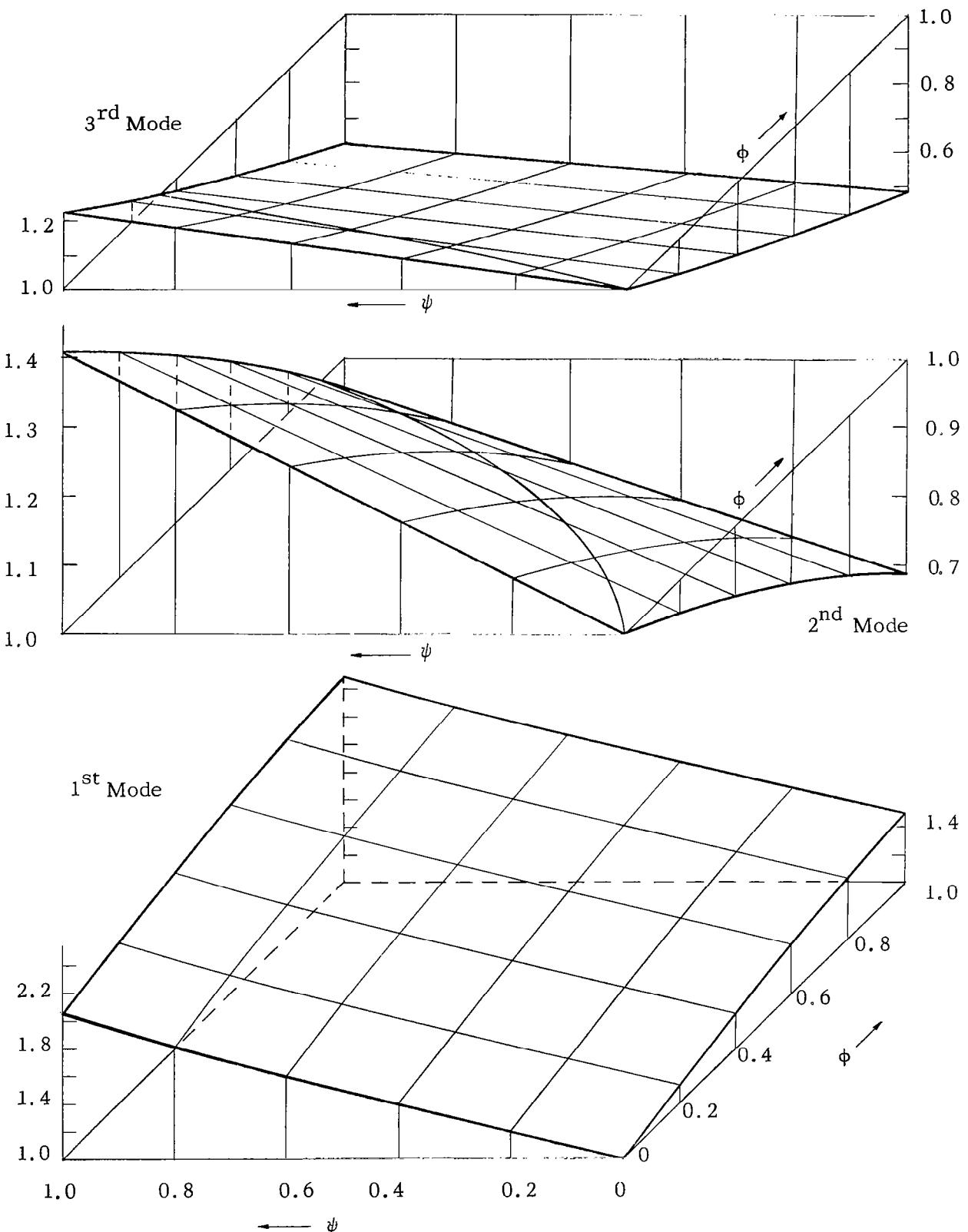


Fig. 6 Ratio of Frequencies of Tapered Cantilever Beams
to Frequencies of a Uniform Beam

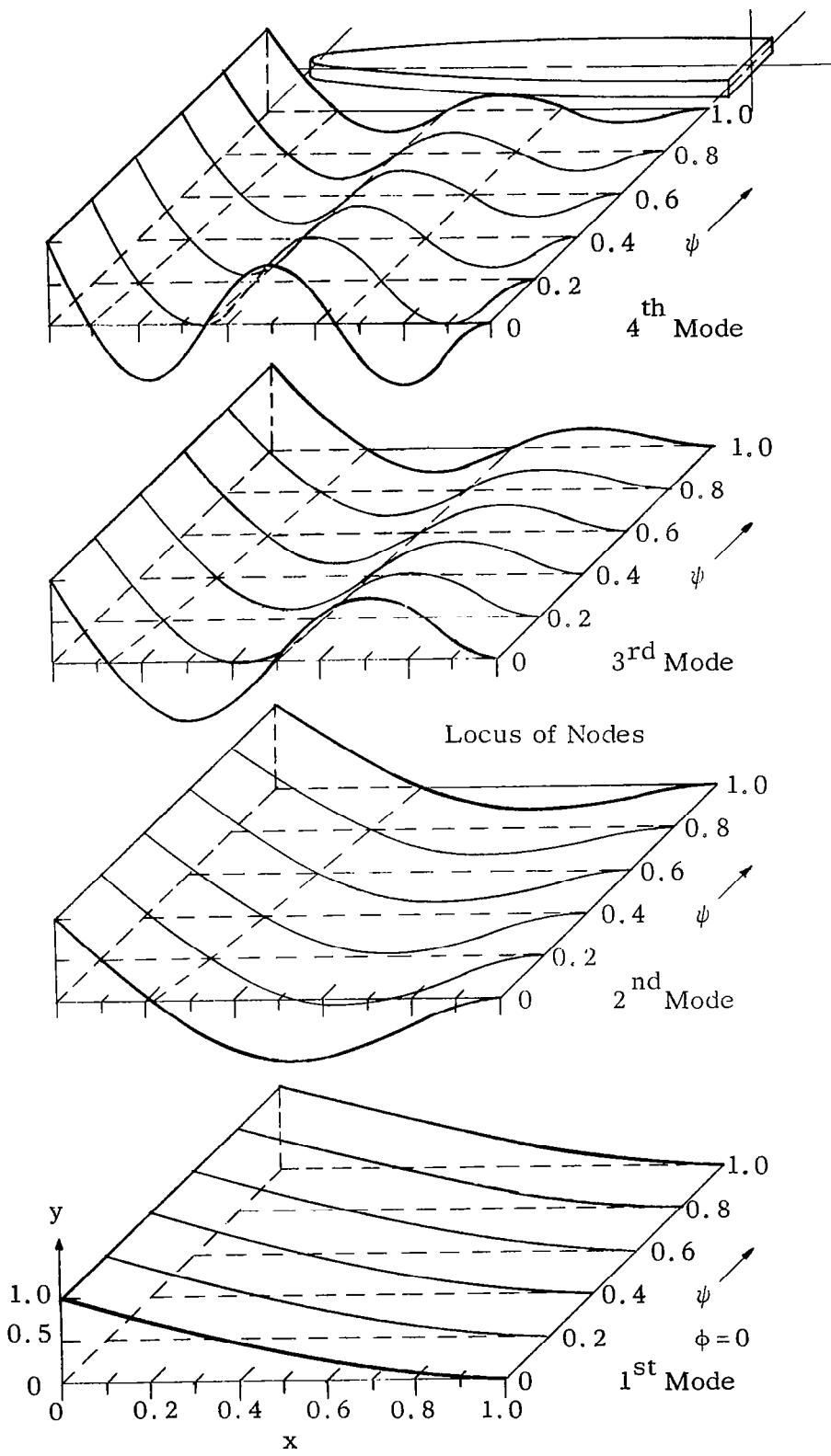


Fig. 7 Mode Shapes for Cantilever Beams with Varying Width and Constant Thickness

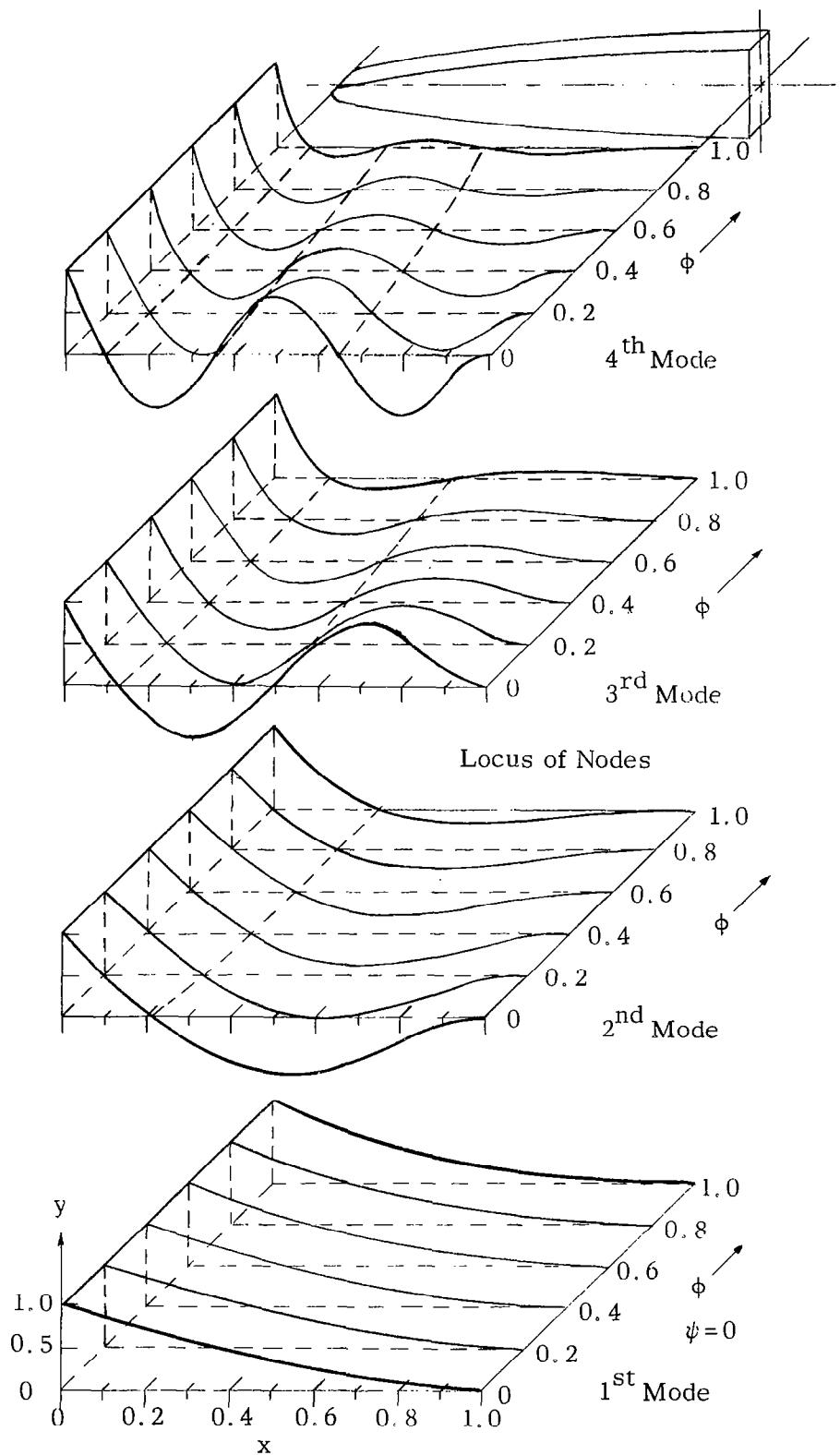


Fig. 8 Mode Shapes for Cantilever Beams with Varying Thickness and Constant Width

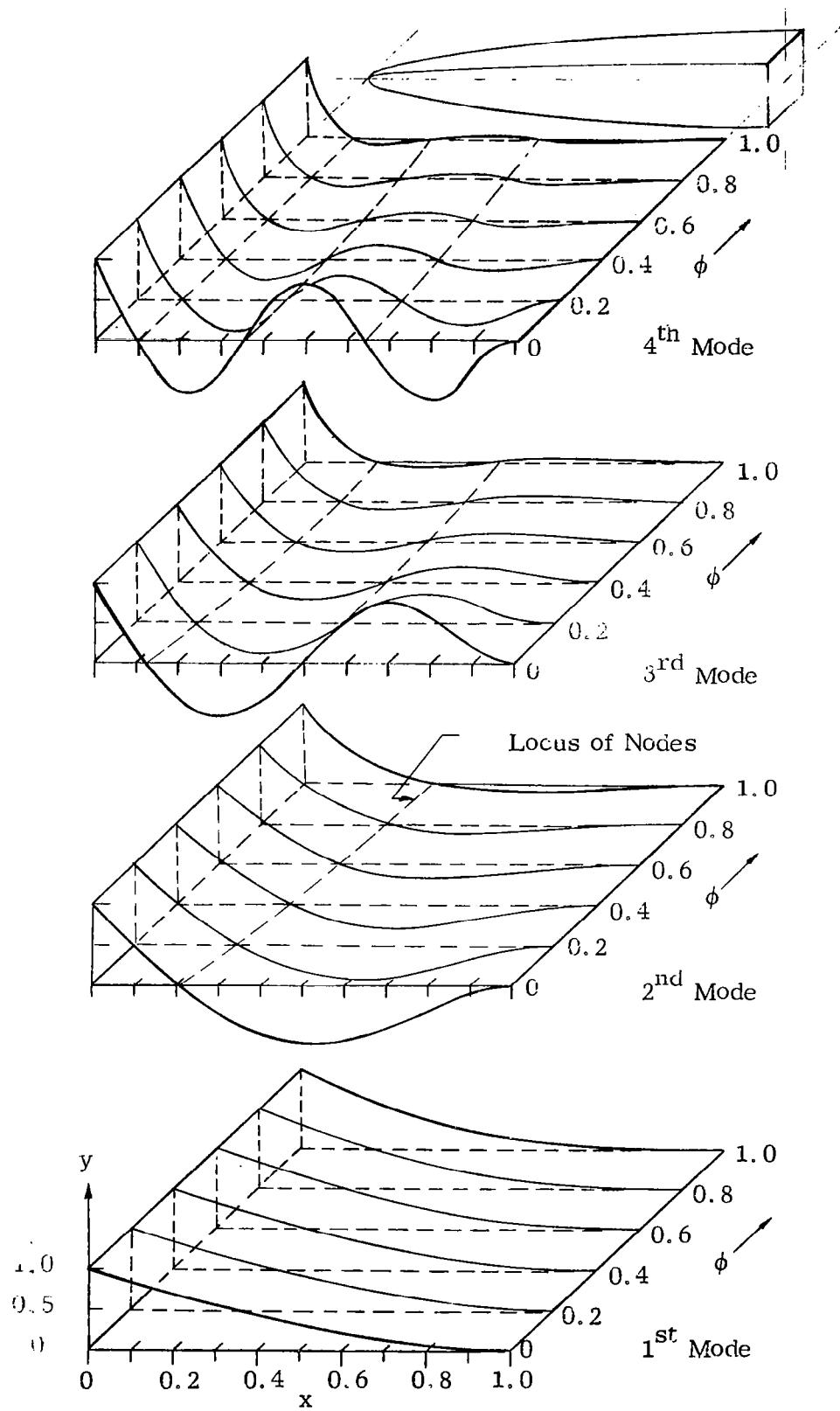


Fig. 9 Mode Shapes for Cantilever Beams with Varying Width and Thickness

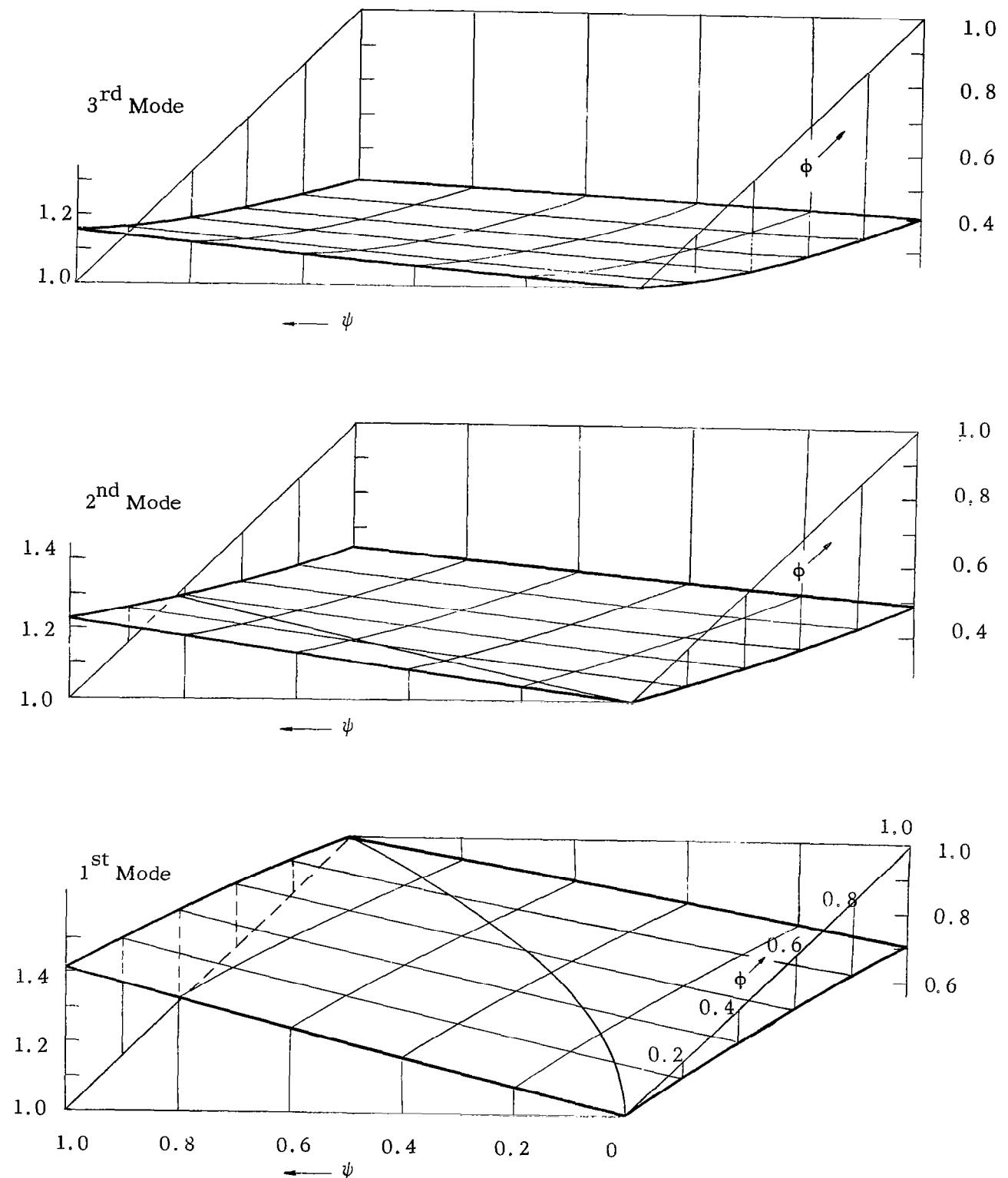


Fig.10 Ratio of Frequencies of Antisymmetrical Mode of Tapered Free-Free Beams to Frequencies of a Uniform Beam

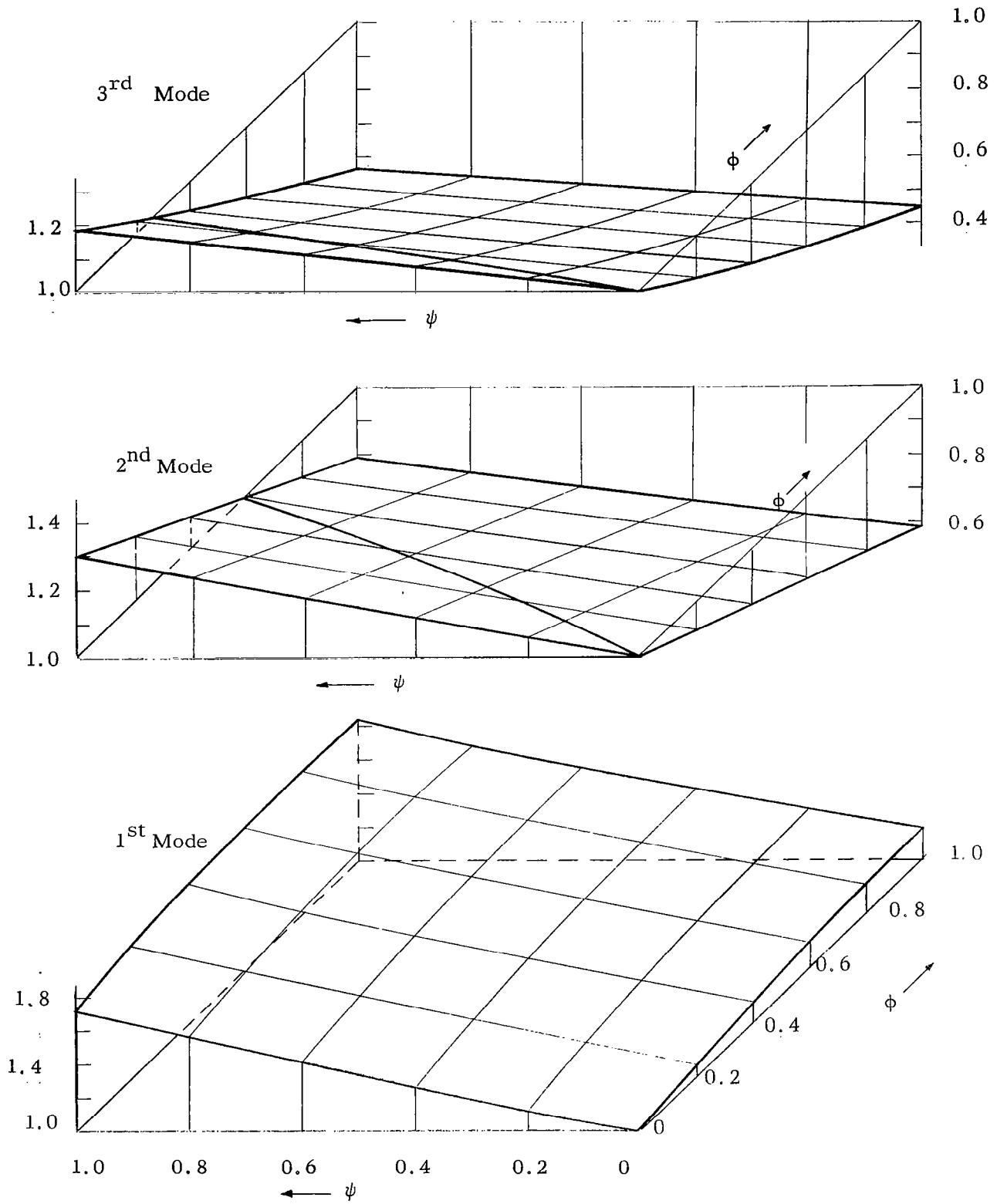


Fig. 11 Ratio of Frequencies of Symmetrical Mode of Tapered Free-Free Beams to Frequencies of a Uniform Beam

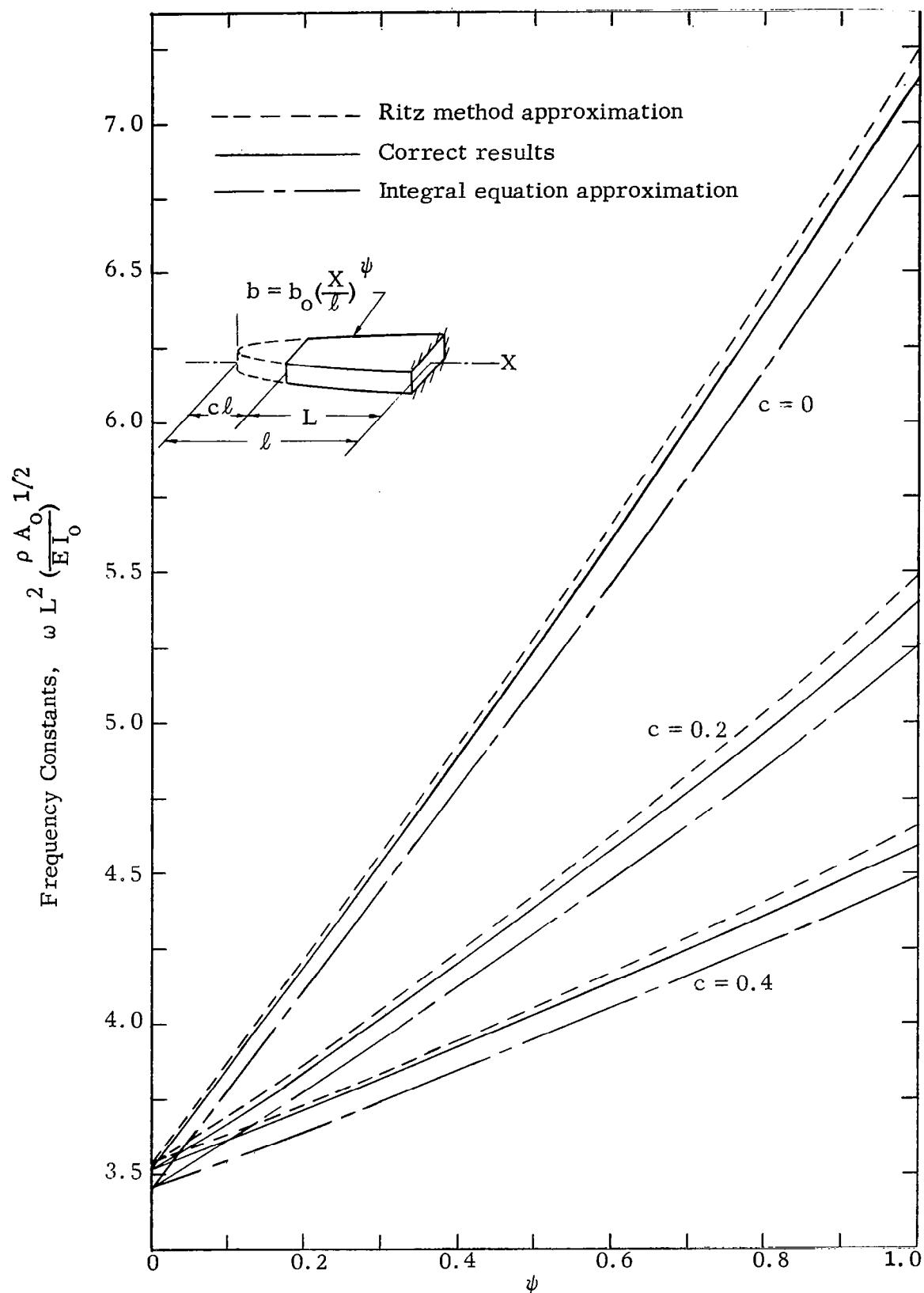


Fig.12 Fundamental Frequencies of Truncated Cantilever Beams with Varying Width

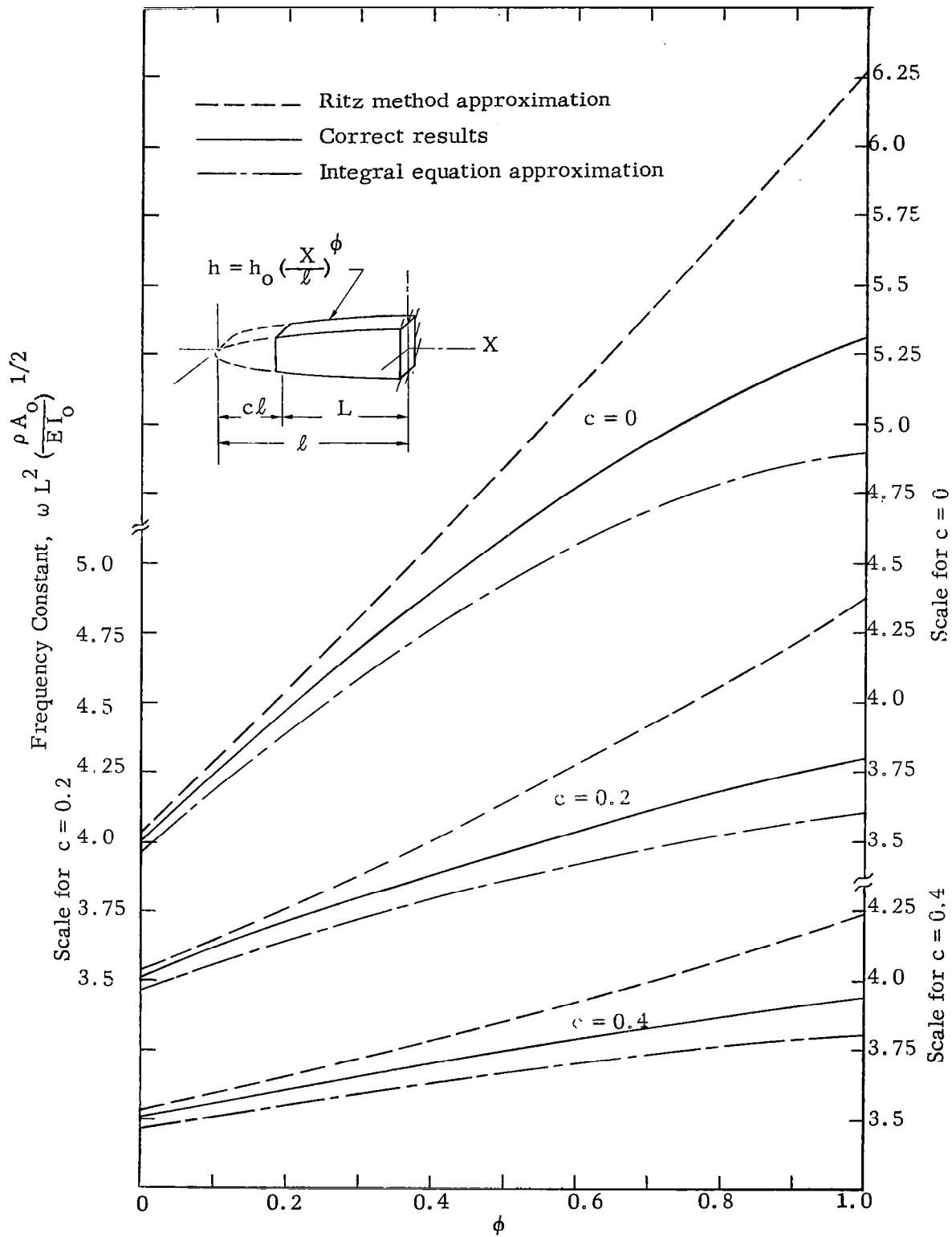


Fig. 13 Fundamental Frequencies of Truncated Cantilever Beams with Varying Thickness

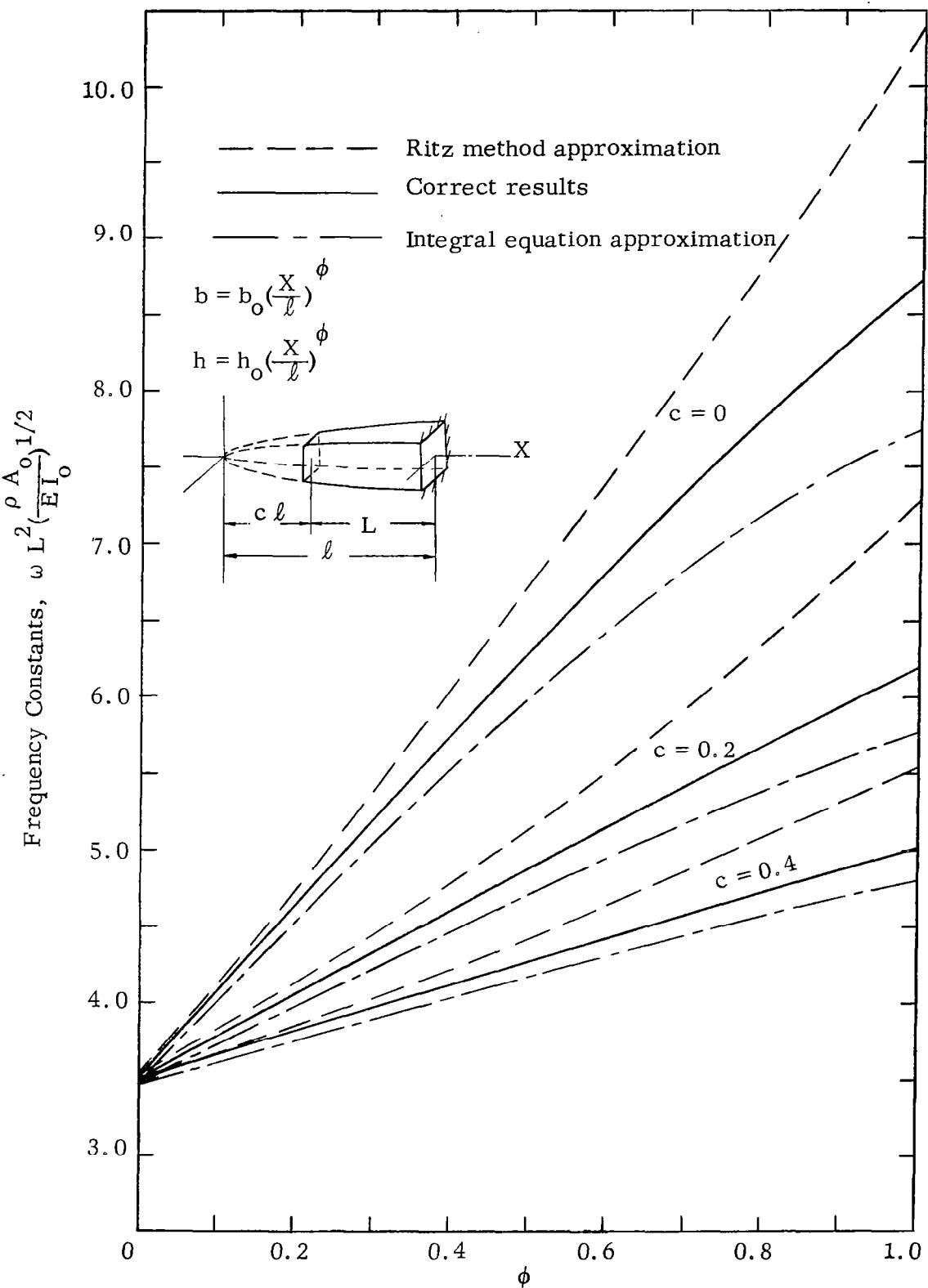


Fig. 14 Fundamental Frequencies of Truncated Cantilever Beams with Varying Width and Thickness